# Turbulent Flow Induced by Oscillatory Circular Cylinder Arrays

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- Vegetation association plays important role in the shallower coastal zone
  - for sediment control
  - the nutrient
  - carbon absorption
  - etc.
- Evaluation of shallow water region including vegetation and wet land

need to understand the fluid motion including turbulence in the vegetation association







- The first step for understanding fluid motion in the vegetation association
  - fluid force acting on a circular cylinder
  - fluid motion around a circular cylinder
  - visualization is useful tool to overview the fluid motion







#### ✓ Zhida Yuan & Zhenhua Huang(2015)

- <u>Hydrodynamic coefficients of the transverse force</u> on a circular cylinder oscillating sinusoidally in still water
- ✓ Kuifeng Zhao, Nian-Sheng Cheng, Zhenhua Huang(2014)
  - Experimental study of <u>free-surface fluctuations in open-channel flow</u> in the presence of periodic cylinders array.
- ✓ K. M. Lam, J. C. Hu, and P. Liu(2010):
  - Vortex formation processes from an oscillating circular cylinder
- ✓ M. Tatsuno, P. W. Bearman(1990):
  - A visual study of the flow around an oscillating circular cylinder at low Keulegan-Carpenter numbers and low Stokes numbers



- The properties of turbulent flow induced around circular cylinders in wave field have not been investigated
  - turbulence transition mechanism
  - spatial-temporal distribution of turbulence

# Purpose of this study

- Understanding the fluid motion including turbulence induced by wave transmitting vegetation association.
  - using the PTV technique measuring fluid motion induced by oscillating circular cylinder arrays.



- ✓ Tank : 1.6 m x 0.54 m x 0.4 m
- ✓ Water depth : 0.2 m
- ✓ Cylinder arrays : rotation of a crank disk





- ✓ Cylinder arrays :
  - d : cylinder diameter d = 0.49 m
  - DX : distance between arrays in oscillatory direction DX / d = 2.00, 2.50, 2.78, 3.00
  - *DY* : distance between cylinders in an array

DY/d = 1.24, 1.65, 2.49

arrangement: in-line & staggered





	$V_0$	Arrangement	DX/d	DY/d	$\epsilon$	$T[\mathbf{s}]$	$V_0 [{\rm m/s}]$	$V_g [{\rm m/s}]$	KC	$Re_g$
	$V_g = - \epsilon$	in-line	2.00	1.65	0.40	7.4	0.060	0.150		8,952
	DY - d			2.49	0.60	3.7	0.120	0.200		10,687
	$\epsilon = \frac{DT}{DY}$ $KC = \frac{V_0 T}{d}$ $Re_g = \frac{V_g d}{\nu}$ $V \longleftarrow Cylinders$			1.65	0.40	4.9	0.090	0.225	0.0	13,429
				1.65	0.40	3.7	0.120	0.300	9.0	17,905
				1.65	0.40	3.0	0.148	0.370		22,083
				1.24	0.19	3.7	0.120	0.632		38,741
				2.49	0.60	5.3	0.120	0.200		10,687
				1.65	0.40	5.3	0.120	0.300	13.0	17,905
				1.24	0.19	5.3	0.120	0.632		38,741
				2.49	0.60	7.0	0.120	0.200		10,687
				1.65	0.40	7.0	0.120	0.300	17.1	17,905
				1.24	0.19	7.0	0.120	0.632		38,741
	FOV		2.50	2.49	0.60	3.7	0.120	0.200		10,687
				1.65	0.40	3.7	0.120	0.300	9.0	17,905
				1.24	0.19	3.7	0.120	0.632		38,741
	V		3.00	2.49	0.60	3.7	0.120	0.200		10,687
	y y g			1.65	0.40	3.7	0.120	0.300	9.0	17,905
				1.24	0.19	3.7	0.120	0.632		38,741
		staggered	2.00	1.65	0.40	7.4	0.060	0.150		7,836
						4.9	0.090	0.225	0.0	11,754
						3.7	0.120	0.300	5.0	15,672
						3.0	0.148	0.370		19,328
						5.3	0.120	0.300	13.0	15,672
						7.0	0.120	0.300	17.1	15,672
*										8

### Experimental setup

- ✓ PTV measurement
  - continuum laser light sheet
  - capture interval
    - 1/200 s
  - exposure time
    - 1/200 s
  - spatial resolution
    - 1.2x10<sup>-2</sup> cm/pixel
  - tracer number density
    - 30 # / cm<sup>2</sup>
  - algorithm
    - PLCV(path line connecting velocimetry, Umase et.al.; 2011)





#### ✓ path line connecting method (Umase et. al., 2011)





 Velocities on the regular grid points were obtained by spatial-averaging measured velocities in a control volume with an certain diameter

$$\boldsymbol{v}_S(x_c, y_c) = \sum_{m=1}^M \boldsymbol{v}_m(x_m, y_m)/M$$

*M* : number of measured velocities in control volume with an certain diameter





- ✓ Distribution of
   Velocity : v<sub>s</sub>
  - in-line
  - DX/d=2.0
  - DY/d = 1.65
  - *KC*=9.0
  - $Re_{g}$ =10,687







- ✓ Distribution of
   Velocity : v<sub>s</sub>
  - staggered
  - DX/d = 2.0
  - DY/d = 1.65
  - *KC*=9.0
  - $Re_{g} = 15,672$

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# Results

✓ Time-averaged velocity over a period :  $\overline{v_s}$ 

$$\overline{oldsymbol{v}_S} = rac{1}{T} \int_0^T oldsymbol{v}_S dt$$

- DX/d=2.0
- DY/d=1.65
- *KC*=9.0





# Results

✓ Time-averaged velocity over a period :  $\overline{v_s}$ 

$$\overline{\boldsymbol{v}_S} = \frac{1}{T} \int_0^T \boldsymbol{v}_S dt$$

- DX/d=2.78
- DY/d=1.84
- *KC*=17.1





✓ Characteristic of time history of velocity :  $v_s$ 

- separations and vortexes are observed
- focus the time variation of spatial averaged velocity  $v_s$  on  $P_A$ ,  $P_B$ ,  $P_C$ ,  $P_D$





- ✓ Characteristic of time history of velocity :  $v_s$ 
  - separations and vortexes are observed
  - focus the time variation of spatial averaged velocity
     v<sub>s</sub> on P<sub>A</sub>, P<sub>B</sub>, P<sub>C</sub>, P<sub>D</sub>
- Different characteristics at the different points around a circular cylinder
  - include strong fluctuation
  - have different phases at different points







✓ Spatial averaged  $v_s$  : < $v_s$ >

$$\langle oldsymbol{v}_S 
angle = \int oldsymbol{v}_S dx dy / (N_x N_y)$$

- DX/d = 2.0
- DY/d = 1.65
- KC = 9.0

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✓ Spatial averaged  $v_s$  : < $v_s$ >

 $\langle \boldsymbol{v}_S 
angle = \int \boldsymbol{v}_S dx dy / (N_x N_y)$ 

- -DX/d = 2.0
- -DY/d = 1.65
- KC = 9.0





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- $\checkmark$  Distribution of  $v_s$ 
  - DX/d = 2.0
  - DY/d = 1.65
  - *KC*=9.0
  - $Re_{g}$ =22,083









# $\checkmark$ Distribution of $v_{s^4}$

- *DX/d=*2.78
- DY/d=1.84
- *KC*=17.1
- $Re_g = 12,319$









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<sup>6</sup> Occurrence of oscillatory flow in the transverse direction of cylinder oscillation under certain conditions





- ✓ Definition of turbulence
  - $v_s' = v_m v_s$
- ✓ Definition of turbulence energy
  - $-K_s = 0.5 v_s'^2$
  - $\langle K_{s} \rangle^{*} = K_{s} / V_{g}^{2}$







- ✓ Phase variation of  $\langle K_s \rangle^*$ 
  - The larger KC, the smaller the minimum  $\langle K_s \rangle^*$
  - The larger KC, the phase of  $\langle K_s \rangle^*$  tends to shift
  - Deviation of  $\langle K_s \rangle^*$  for in-line larger than for staggered



- ✓ Relation between  $\langle K_s \rangle$  \* and KC
  - min. and average of <*K<sub>s</sub>*>\*
     become smaller as *KC* increase







KC

#### 0.25 Results $<\!K_S\!>_{ m max}$ staggered $<\!K_S\!>_{ m mean}$ 0.20 $\langle K_S \rangle_{\min}$ ✓ Relation between $\langle K_s \rangle^*$ and KC $< K_S > *$ 0.15 - Increase of KC for in-line 0.10 max. become greater 0.05 – Increase of *KC* for staggered max. become smaller 0.00 5 10 15 20 0





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- ✓ Relation between  $\langle K_s \rangle^*$  and Re
  - As *Re* become greater, min. of average of <*K<sub>s</sub>*> become greater and max. becomes much greater





### Conclusions

Flow field in the gap of the oscillating circular cylinders was measured in detail by the PTV under different conditions, distance between cylinders, oscillatory period, *KC*, *Re*.

Velocity field:

- ✓ Complex fluid motion
  - Separations, vortexes, oblique flow, and so on.
  - Different fluid motions were observed under different conditions
     *KC*, *Re*<sub>g</sub>, arrangement of circular cylinders
  - Oscillating flow in the transverse direction of cylinder oscillation was confirmed to be generated under some conditions.



## Conclusions

Turbulence field:

### ✓ Relation between $\langle K_s \rangle^*$ and KC

- For in-line arrangement, maximum value of  $\langle K_s \rangle^*$  become greater as *KC* increases.
- For staggered arrangement, maximum value of  $\langle K_s \rangle^*$  become smaller as *KC* increases.
- For both cases, minimum and average value of become smaller as *KC* increases.

#### ✓ Relation between $\langle K_s \rangle^*$ and Re

- As *Re* become greater, minimum of average value of  $\langle K_s \rangle^*$  become greater and maximum value becomes much greater.



# Thank you for your kind attentions !

