



36TH INTERNATIONAL CONFERENCE ON COASTAL ENGINEERING 2018

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The State of the Art and Science of Coastal Engineering

A new and fully automatic procedure for the identification and coupling of the overtopping events



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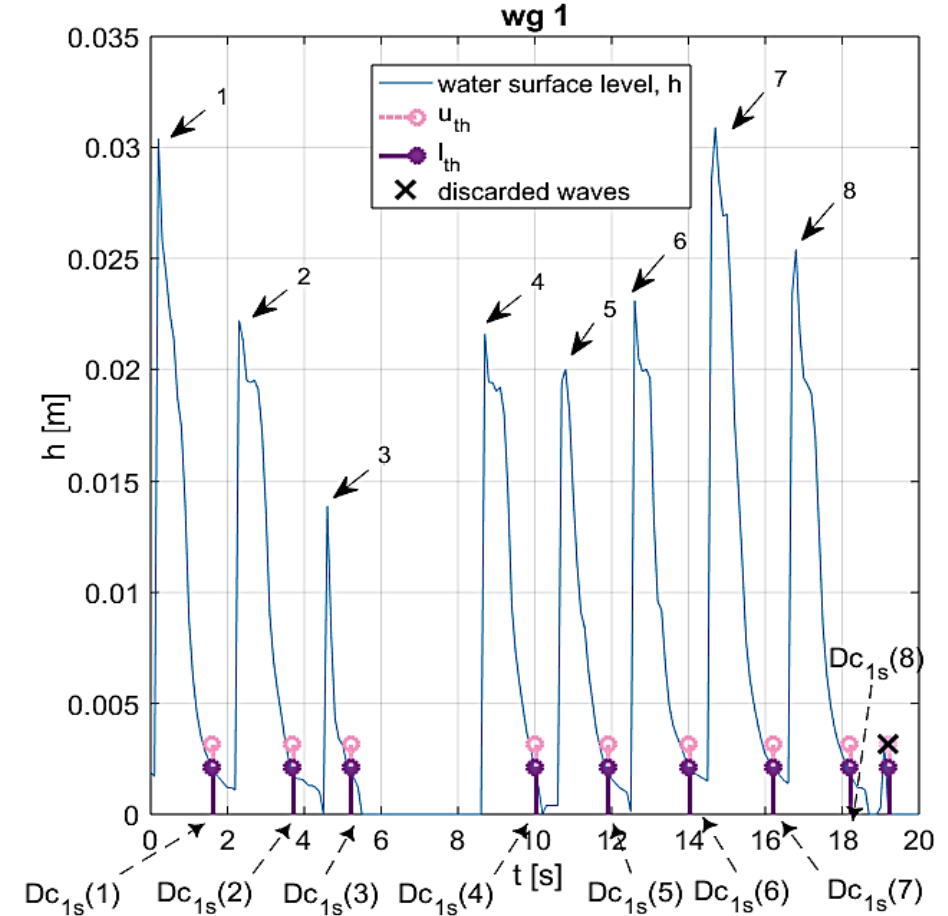
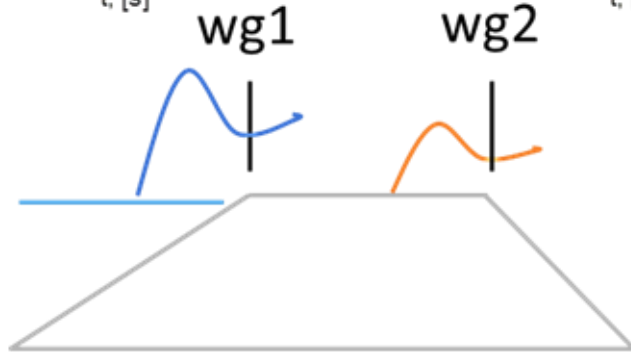
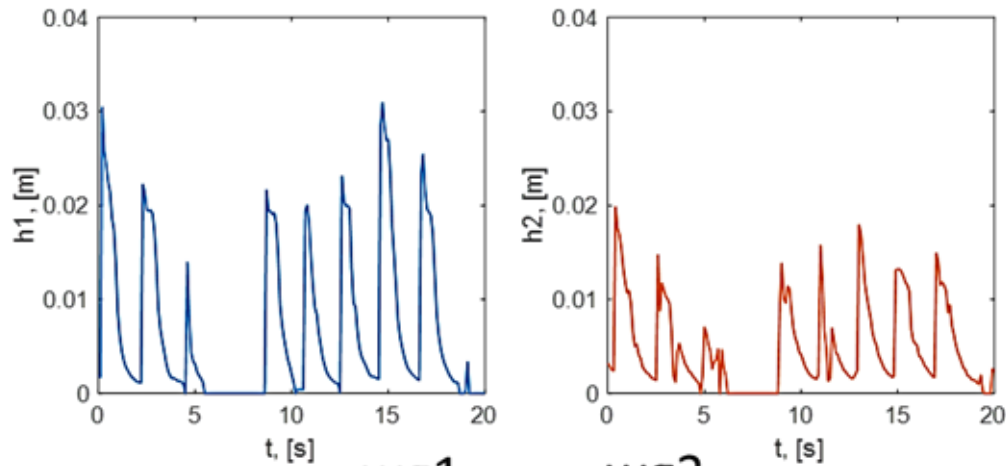
Motivations and background

- Prediction of individual wave overtopping volumes
- Determination of the overtopping flow characteristics across the structure crest
- Assessment of the maximum loads
- Average overtopping discharge



Motivations and background

- Unaffordable inaccuracy of the existing automatic procedures (Hughes & Thornton, 2016)
- No procedure for the coupling of the overtopping events at consecutive gauges exists so far

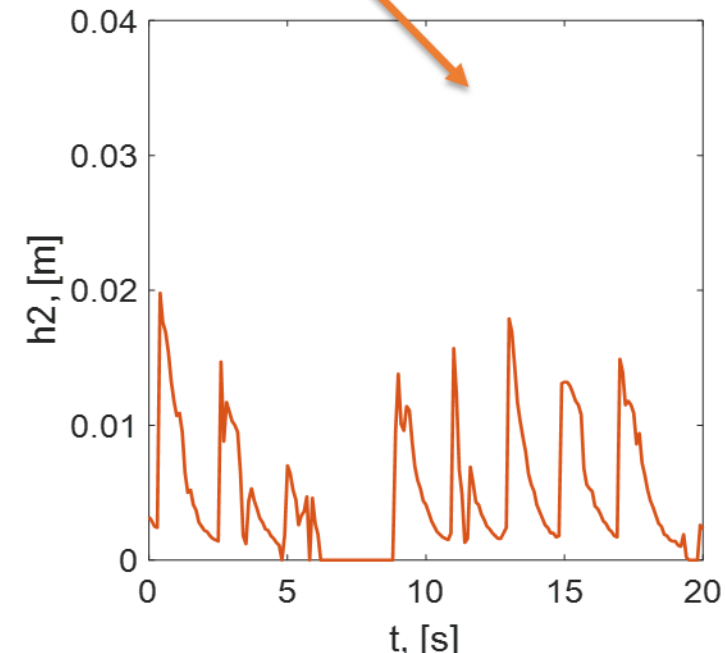
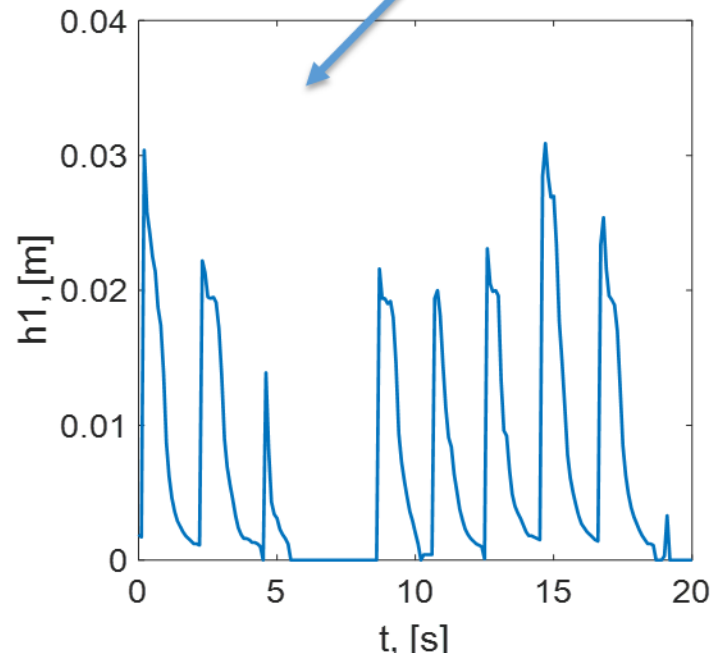
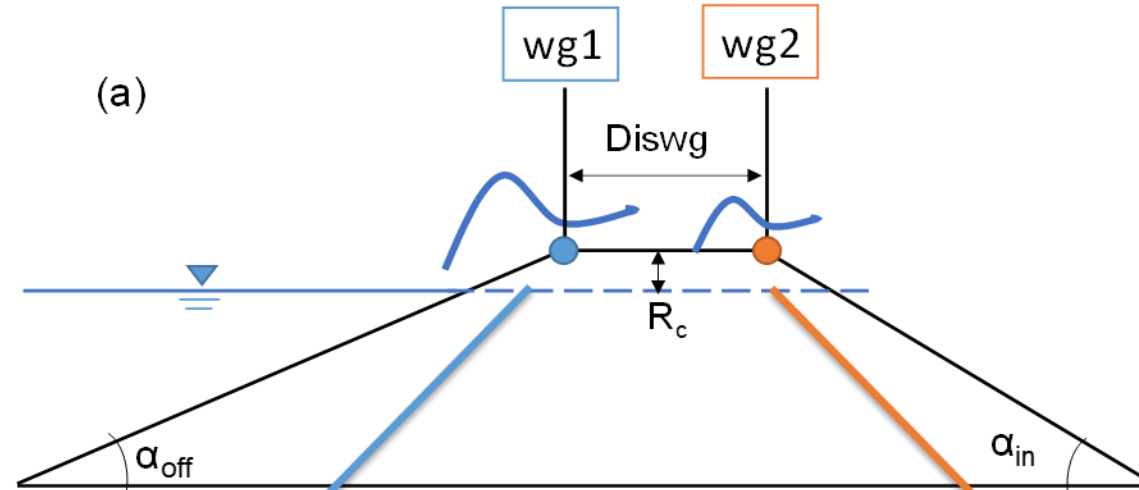


Outline

- Presentation and description of the new procedure
 - First algorithm: the wave identification
 - Second algorithm: the wave coupling
- Benefits and limits of the procedure
 - Rare and frequent overtopping
 - Permeable structures and percolation
- Verification of the procedure
- Applications of the procedure
 - Determination of the extreme wave overtopping volumes
 - Wave celerities
- Conclusions



Scheme and parameters



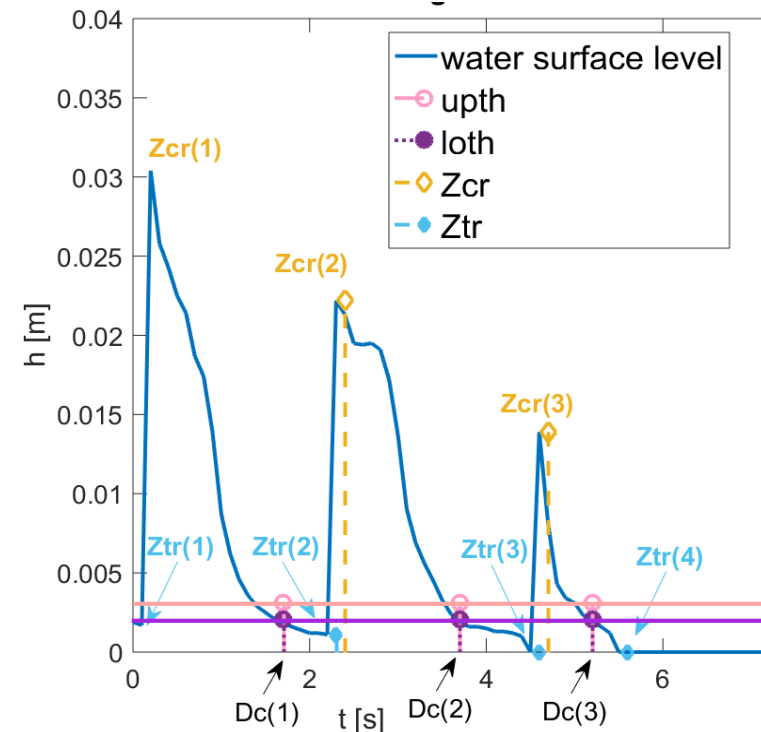
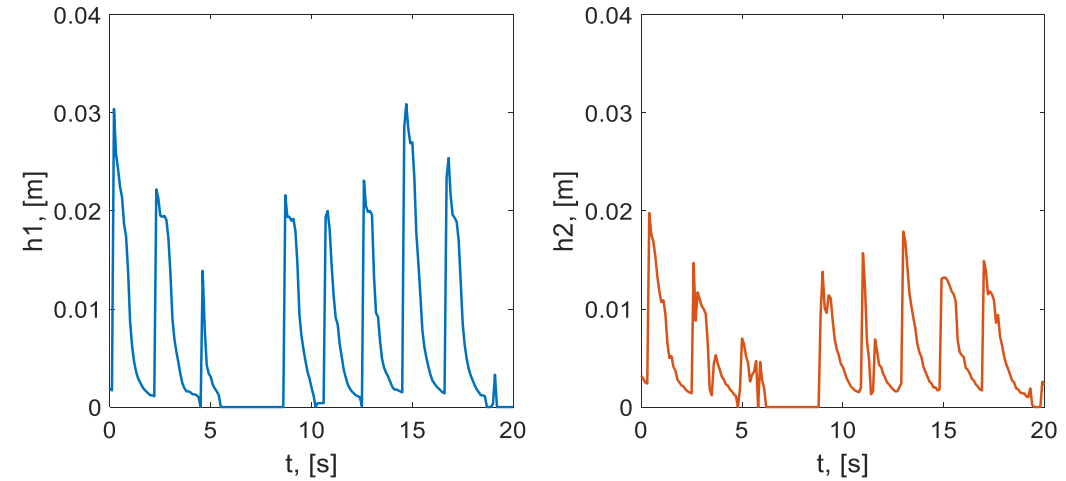
1^o step of the procedure: wave identification

Input 1^o step:
 h_1, h_2 [m]

Definition of the
2 thresholds based on:
 H_s, R_c and diswg

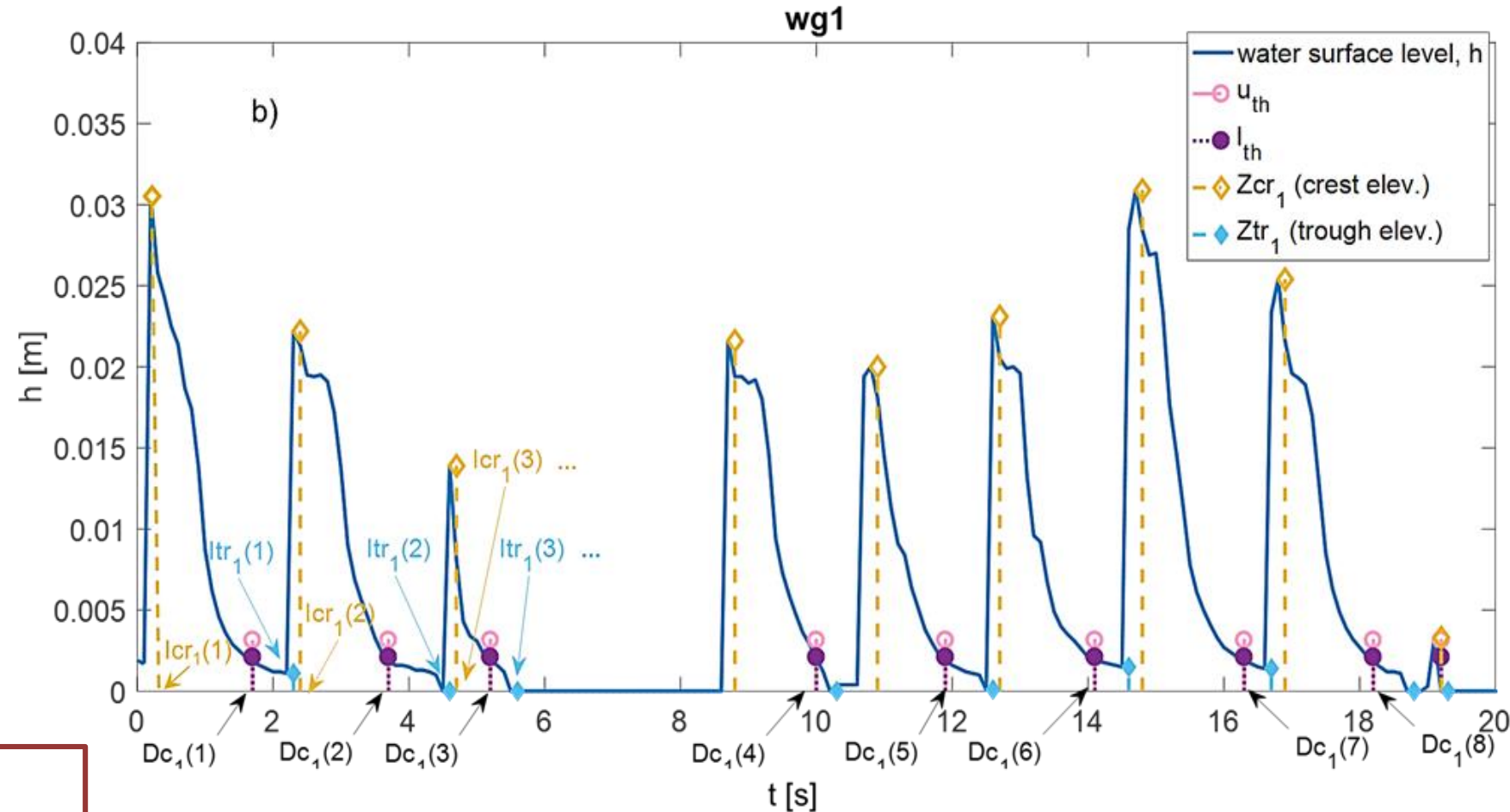
Output 1^o step

- Dc_1, lcr_1, ltr_1 [s] and Zcr_1, Ztr_1 [m]
- Dc_2, lcr_2, ltr_2 [s] and Zcr_2, Ztr_2 [m]



Wave identification: the outputs

- The outputs of the 1st step are the time ordered sequences of:
 - the instants of zero-down-crossing (Dc [s])
 - the instants of occurrence of the wave crests and troughs (lcr , ltr [s])
 - the wave crest and trough heights (Zcr , Ztr [m])



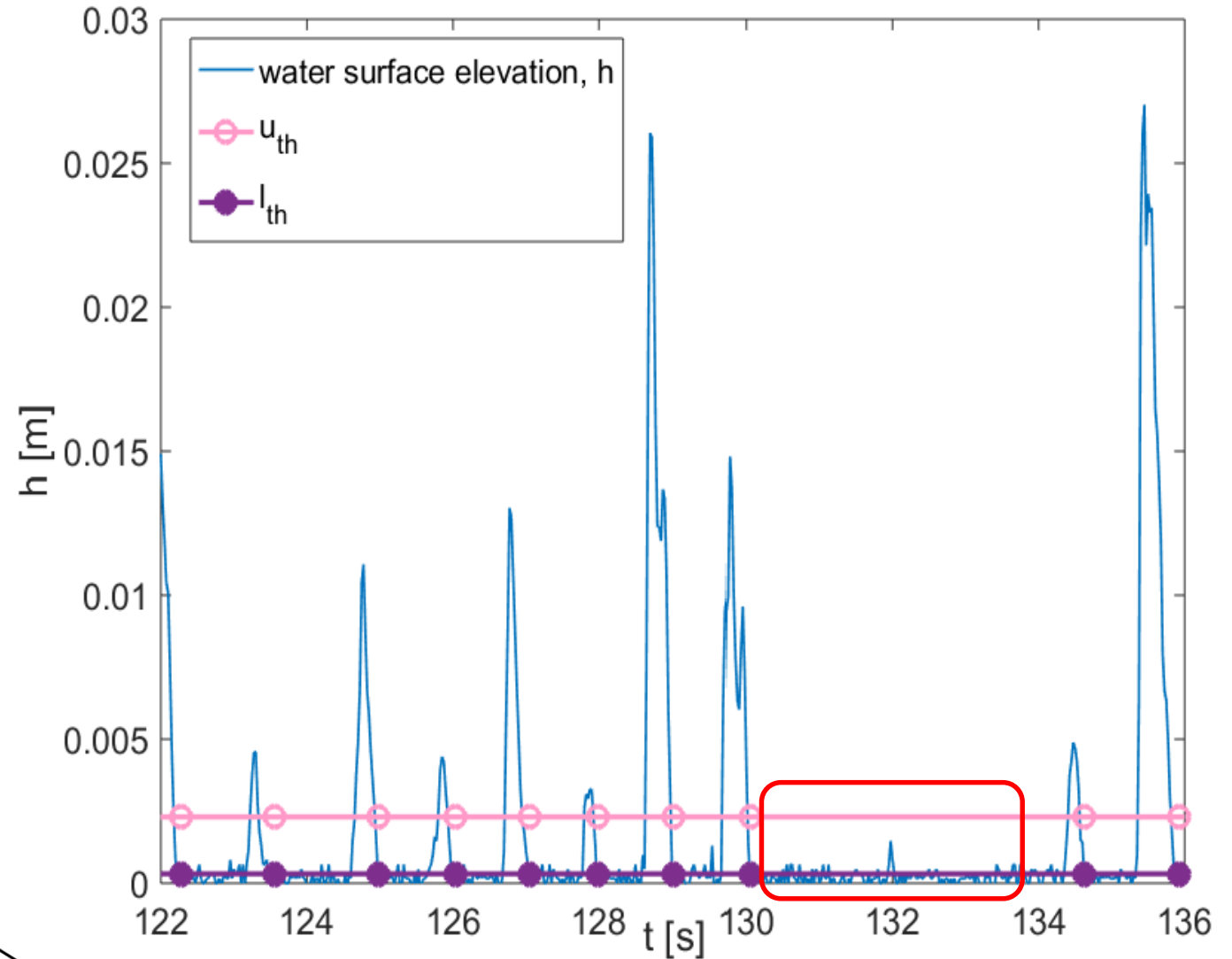
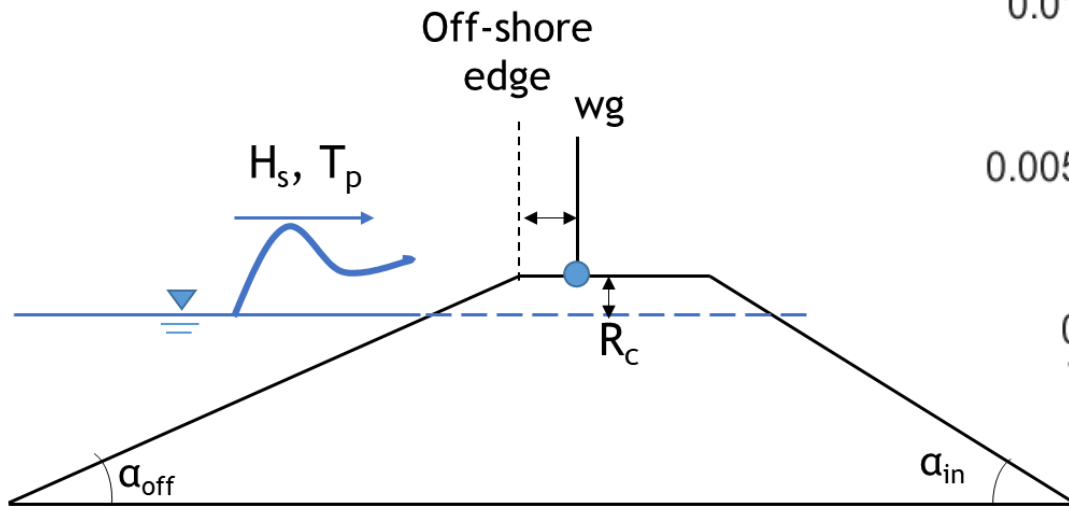
$$H(i) = Zcr(i) - Ztr(i)$$

$$T(i) = Dc(i) - Dc(i-1)$$

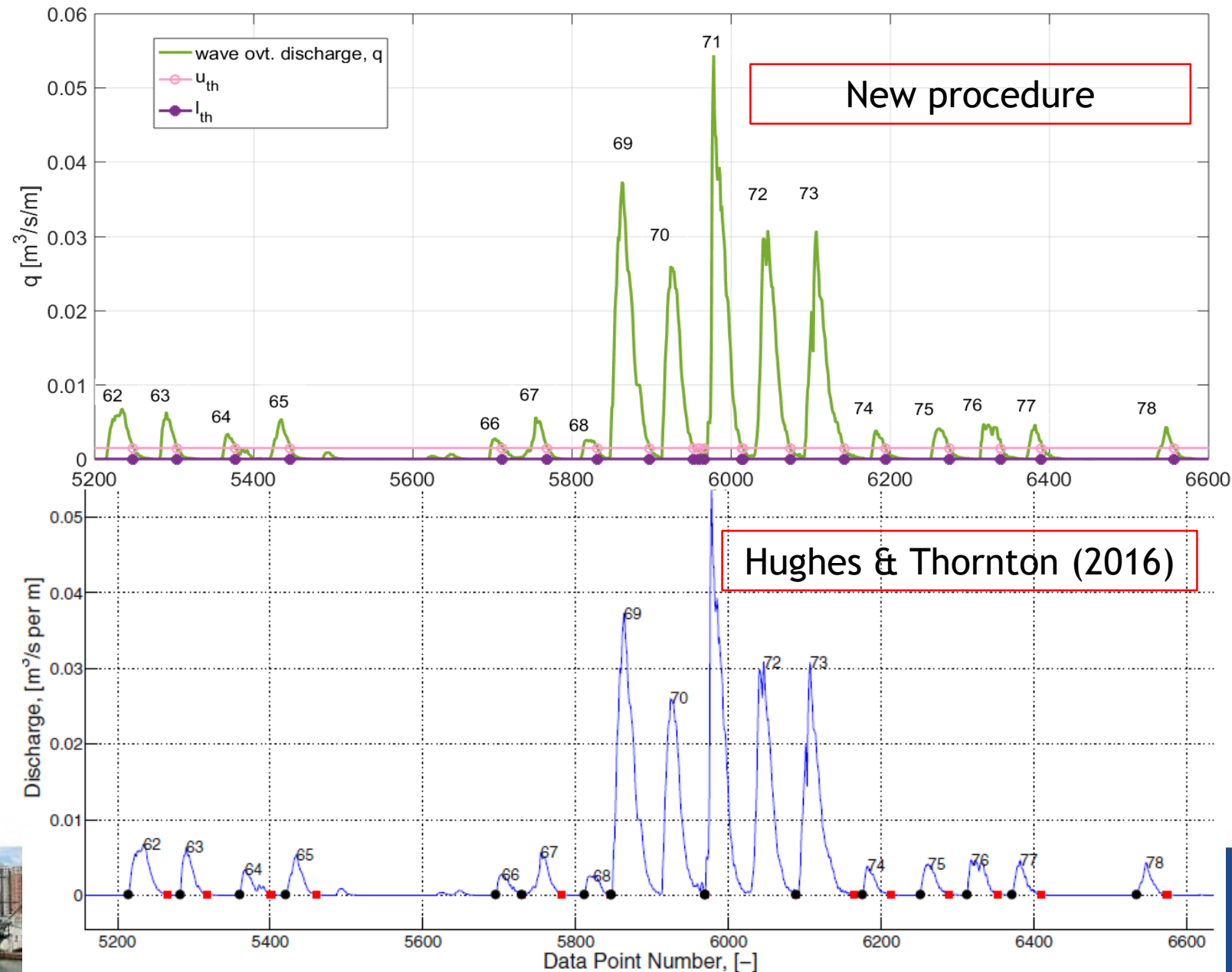


Wave identification: definition of the thresholds

- The thresholds vary with:
 - The structure freeboard (R_c)
 - The wave characteristics (H_s and T_p)
 - The distance of the wg from the dike off-shore edge



Verification of the identification step



Verification of the identification step

Tests parameters				Hughes & Thornton procedure			New procedure				
Test ID	H_{m0} [m]	$T_{m-1,0}$ [s]	Nw [-]	Auto. V	Man. V	Total V_{HT}	Auto/Total V_{HT}	P_{ovt}	Auto. V	Auto/Total V_{HT}	P_{ovt}
0198	0.103	1.619	1180	486	177	663	73%	56%	636	96%	54%
0199	0.094	1.164	1102	211	235	446	47%	40%	356	80%	31%
0200	0.15	1.96	1276	453	361	814	56%	64%	839	103%	66%
0201	0.148	1.379	1150	254	493	747	34%	65%	680	91%	59%
0451	0.09	1.555	1097	535	46	581	92%	53%	621	107%	57%
0453	0.122	1.663	1120	726	142	868	84%	78%	931	107%	83%
0456	0.157	1.936	1093	617	275	892	69%	82%	904	101%	83%
0457	0.141	1.373	1116	521	267	788	66%	71%	794	101%	71%

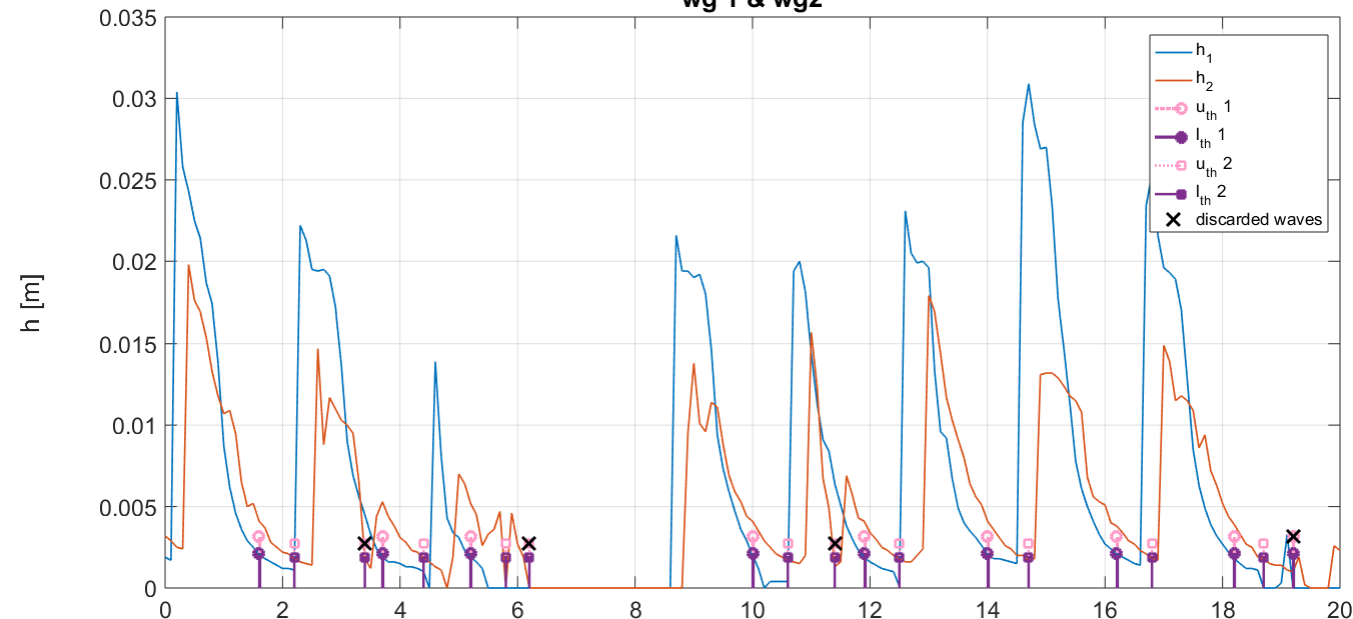
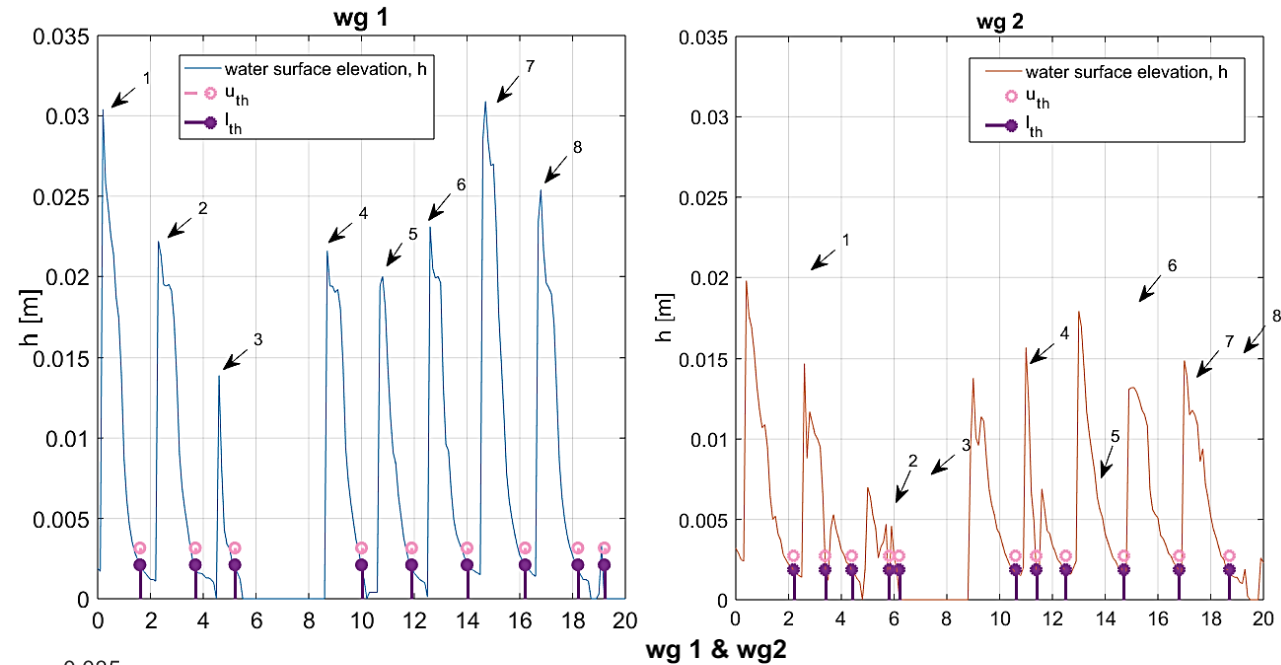


2° step of the procedure: wave coupling

Input 2° step:
 Dc_1 [s] and Zcr_1 [m]
 Dc_2 [s] and Zcr_2 [m]

Definition of the
maximum and minimum
time lags based on:
 H_s , T_p , R_c , $diswg$, sf

Output 2° step
 Dc_{1s} , Dc_{2s} [s]
 Zcr_{2s} , Zcr_{2s} [m]
 c [m/s]

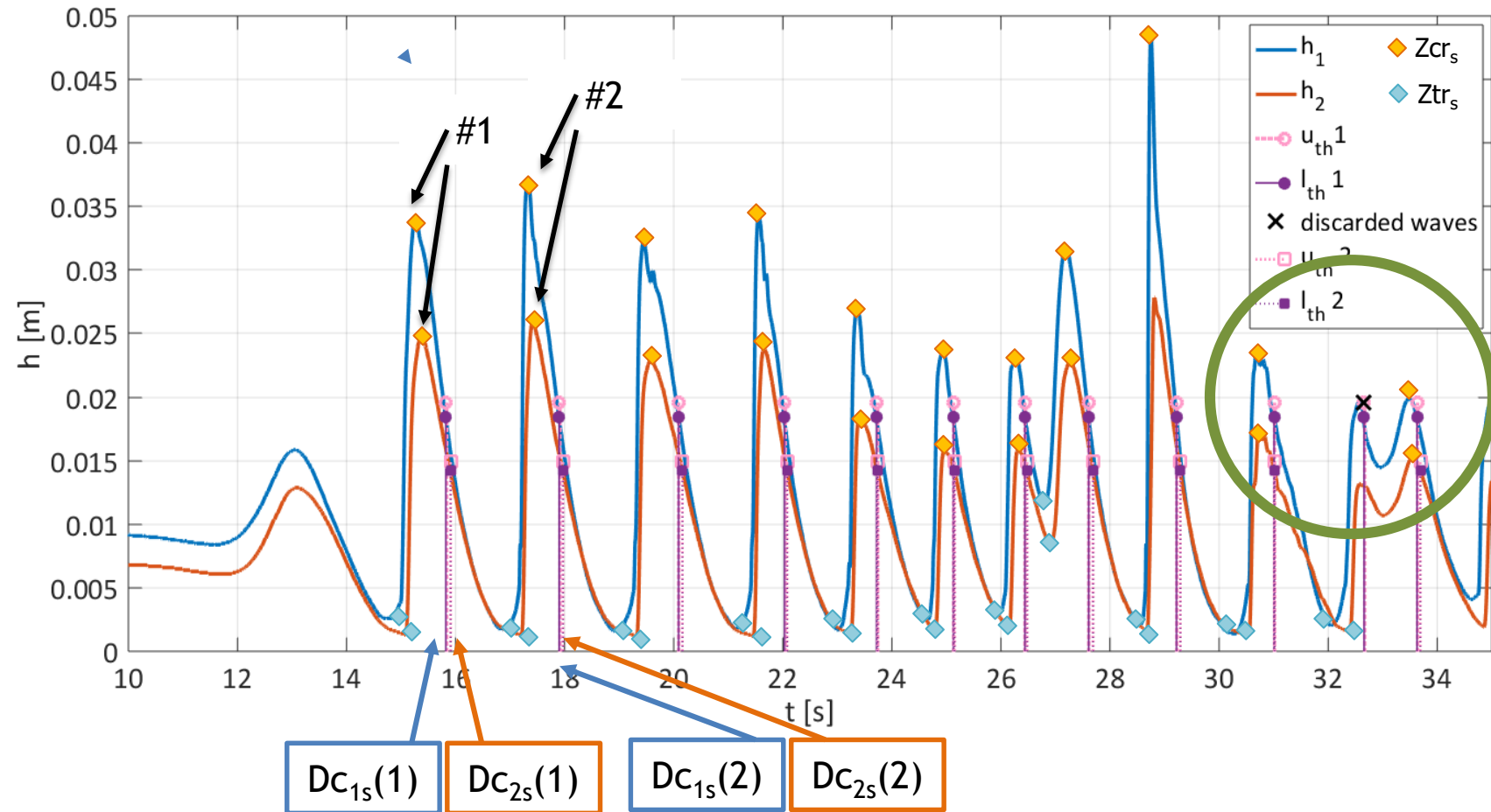


Wave coupling: the outputs

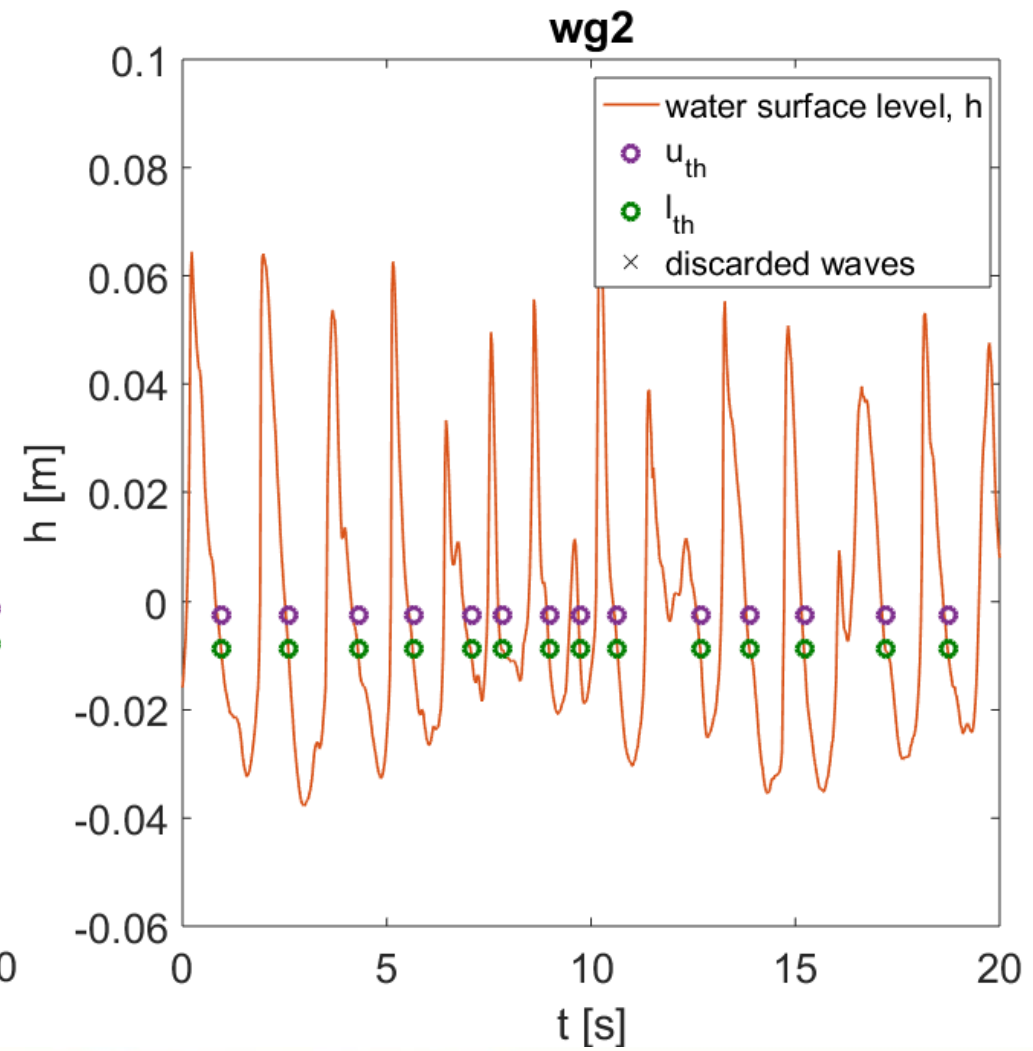
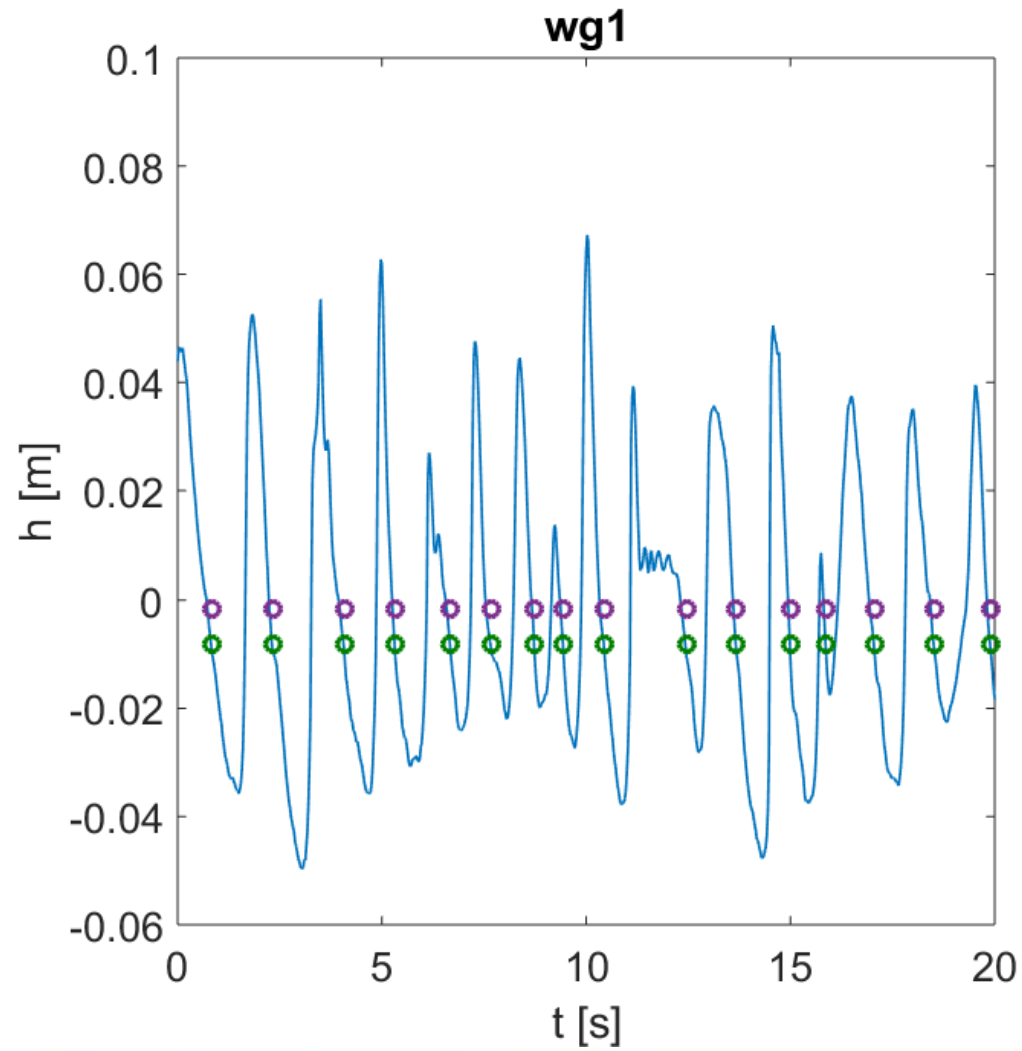
- The outputs of the 2nd step are the time ordered sequences of:

- the instants of zero-down-crossing (Dc_{1s} , Dc_{2s} [s])
- the instants of the wave crests and troughs (Icr_{1s} , Itr_{1s} , Icr_{2s} , Itr_{2s} [s])
- the wave crest and trough heights (Zcr_{1s} , Ztr_{1s} , Zcr_{2s} , Ztr_{2s} [m])

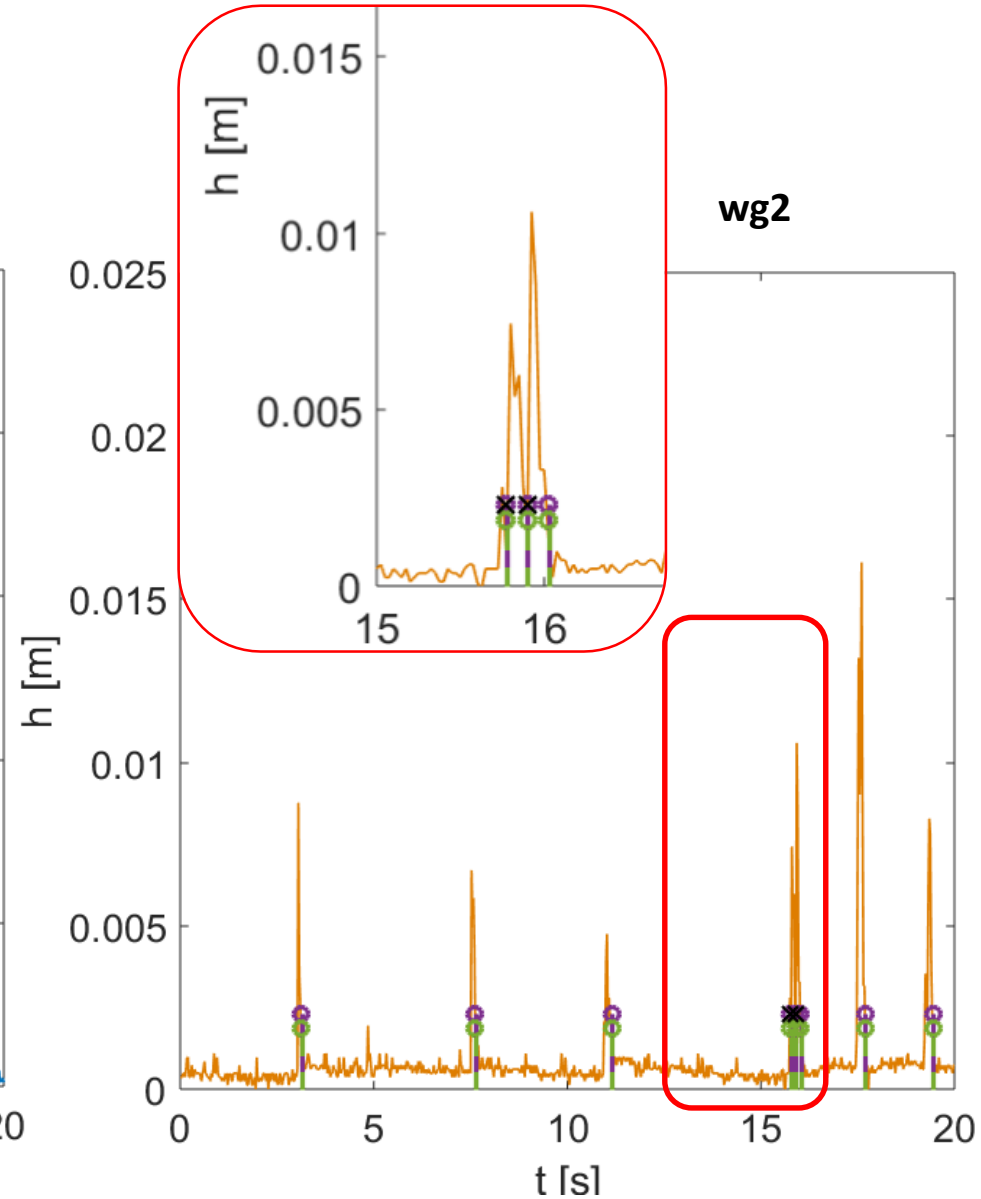
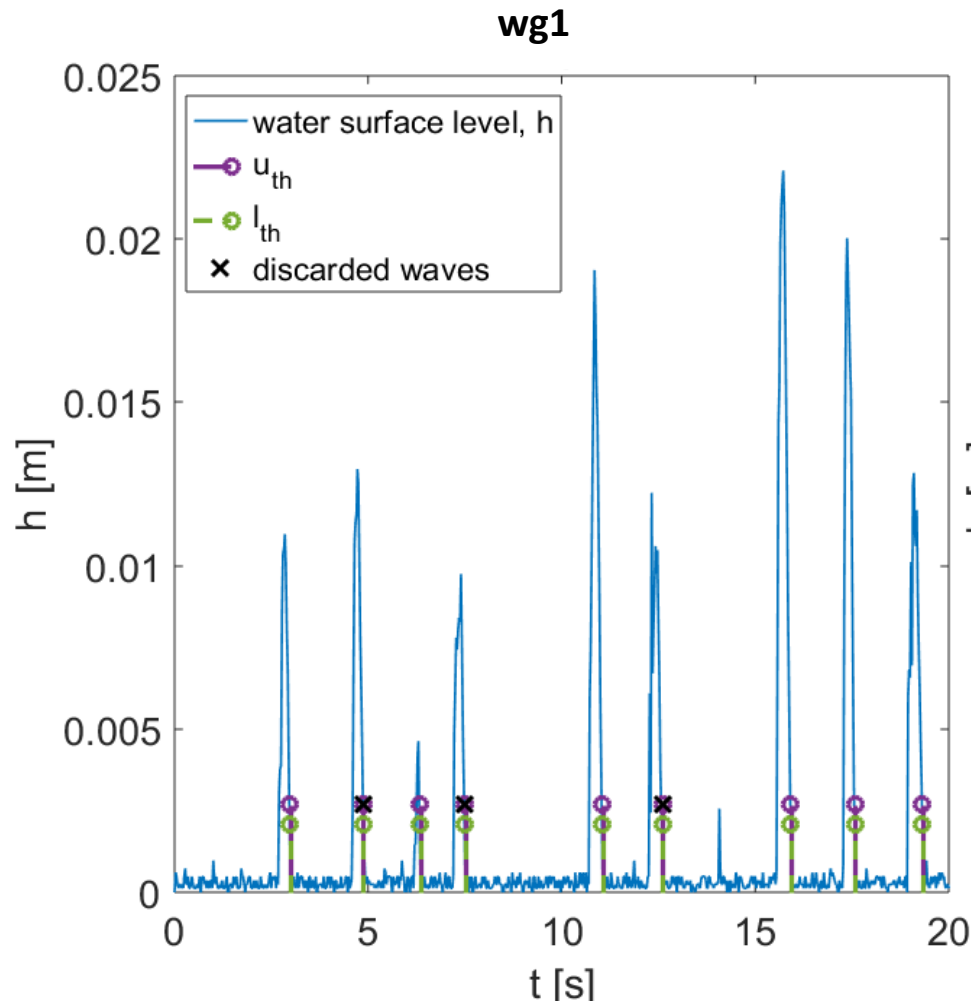
of the coupled events at wg1 and wg2



Frequent overtopping



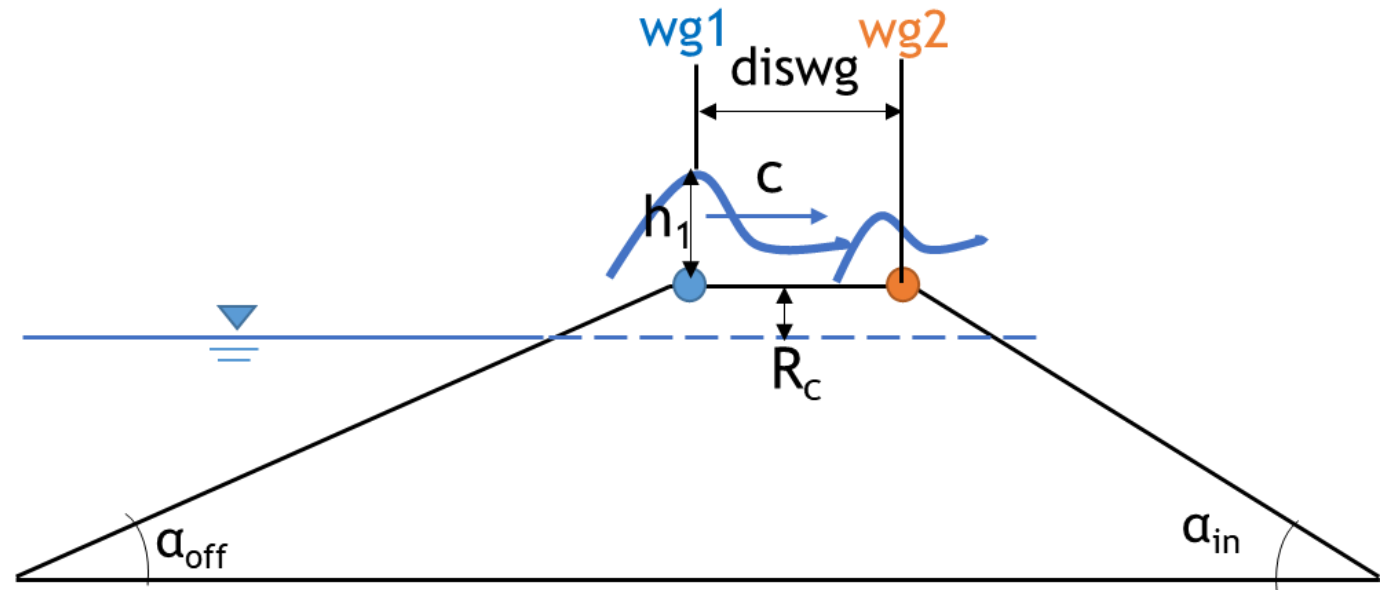
Rare overtopping and percolation



Wave coupling: definition of the time lags

- The max and min time lags vary with:
 - the distance between wg1 and wg2 (diswg, [m])
 - the celerity of the single waves (c, [m/s]); theoretically:
 - c_{\max} in deep water $\rightarrow dt_{\min}$
 - c_{\min} in shallow water $\rightarrow dt_{\max}$
 - the sample frequency of the signals (sf, [Hz])

$$\begin{cases} dt_{\min} = \max\left(\frac{\text{diswg}}{c_{dw}}; \frac{1}{sf}\right), & \text{with } c_{dw} = \frac{L_p}{T_p} \\ dt_{\max} = \frac{\text{diswg}}{c_{sw}}, & \text{with } c_{sw} = \min\left(\sqrt{gh_1}\right) \end{cases}$$



Verification of the coupling step

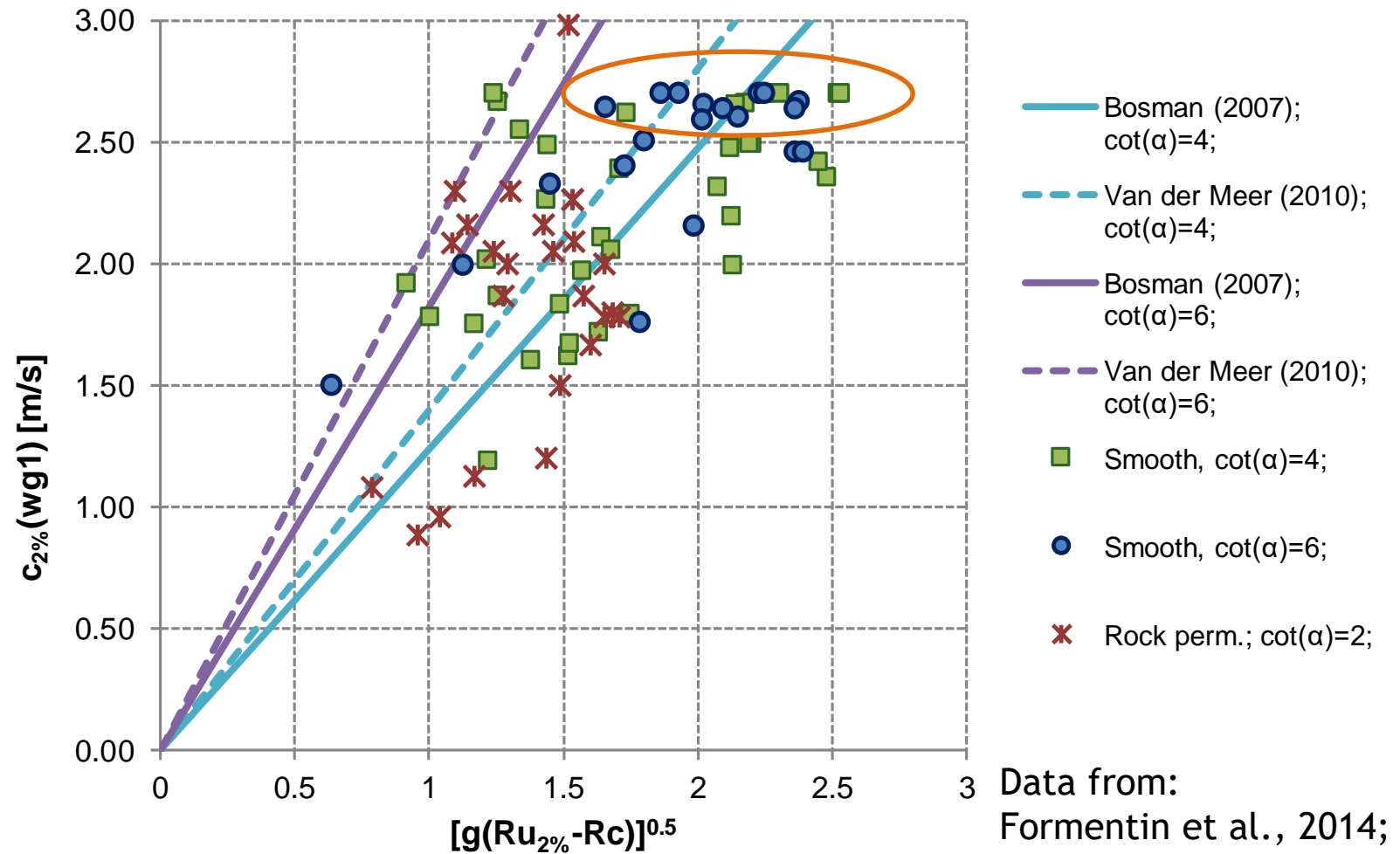
- Determination of the wave celerities:

$$c(i) = \frac{diswg}{Dc2s(i) - Dc1s(i)}$$

- Comparison of the estimated $c_{2\%}$ -values with:

- Bosman et al. (2007);
- Van der Meer et al. (2010)

$$u_{2\%}(x_c) = c_u \cdot [(R_{u,2\%} - R_c)]^{0.5}, \quad R_c \geq 0$$



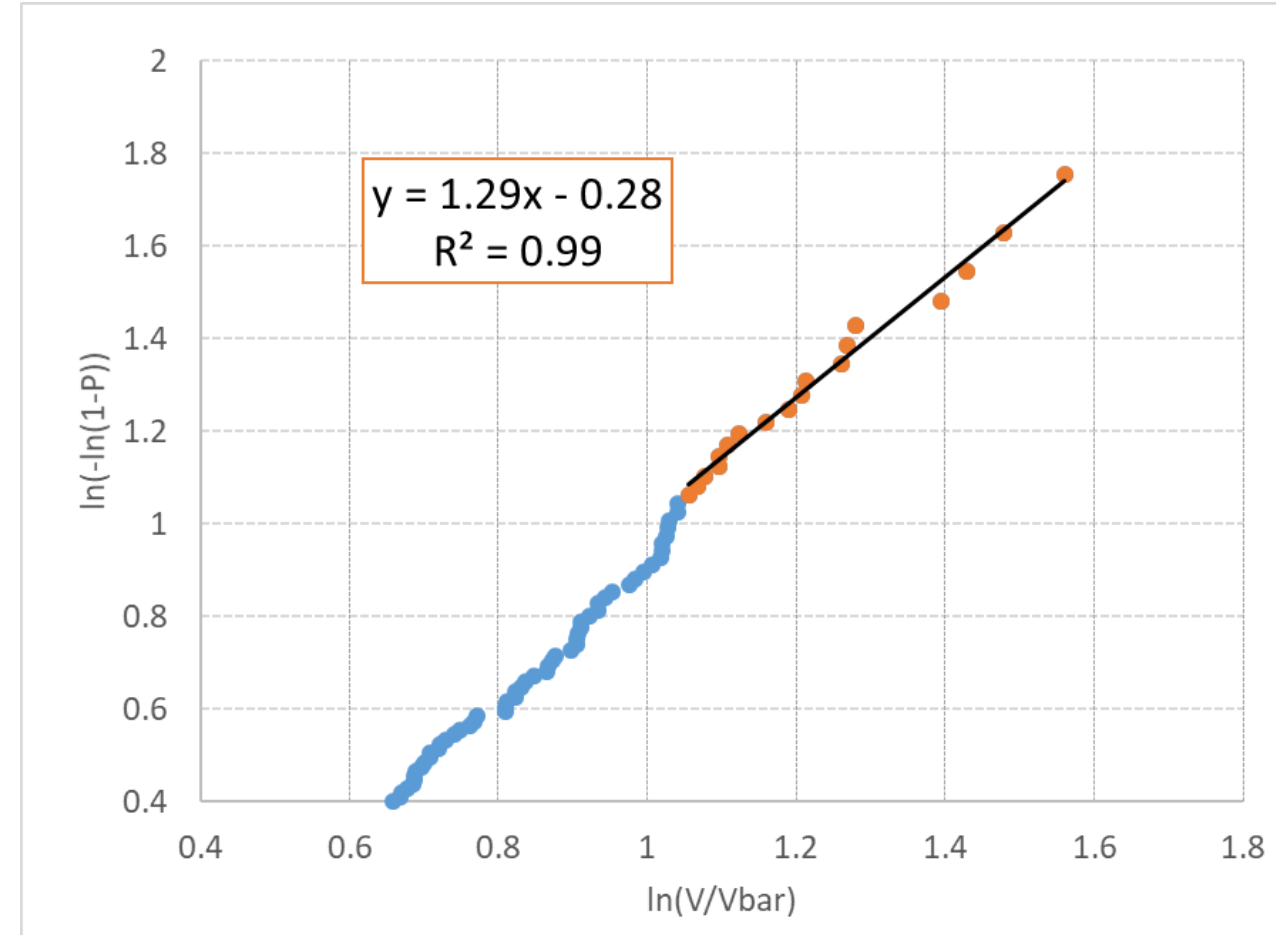
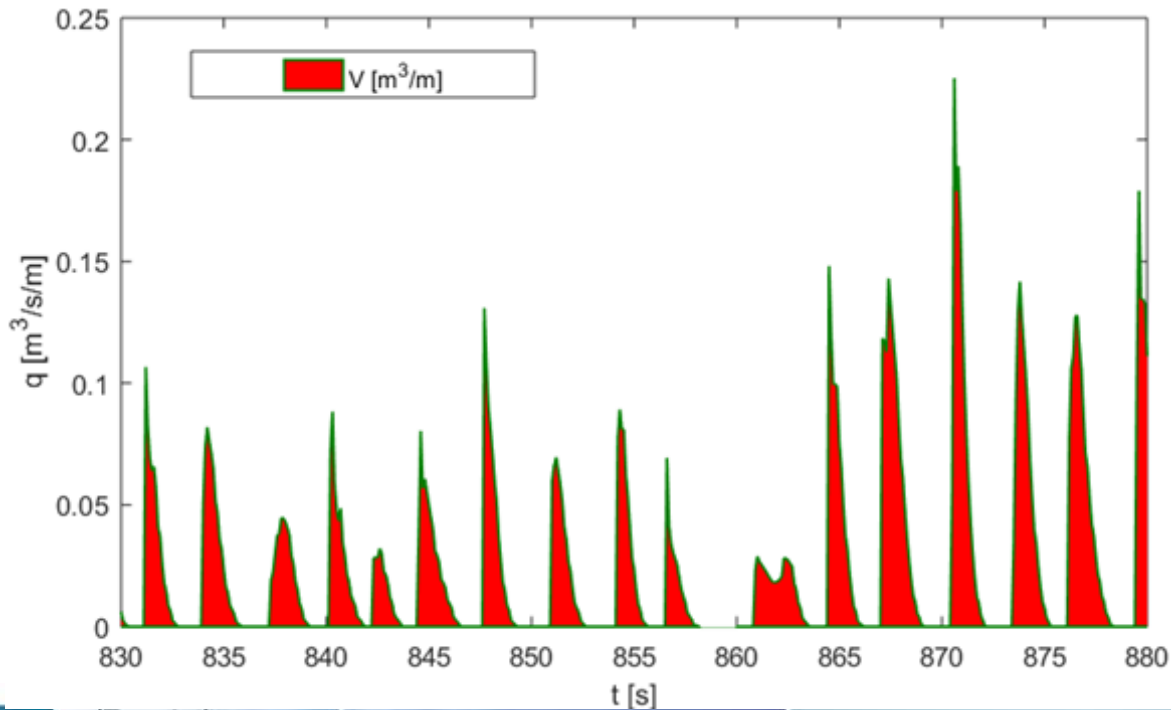
Data from:
Formentin et al., 2014;
Kramer et al., 2005.



Applications: extreme overtopping volumes

- Determination of the Weibull's shape parameter b :

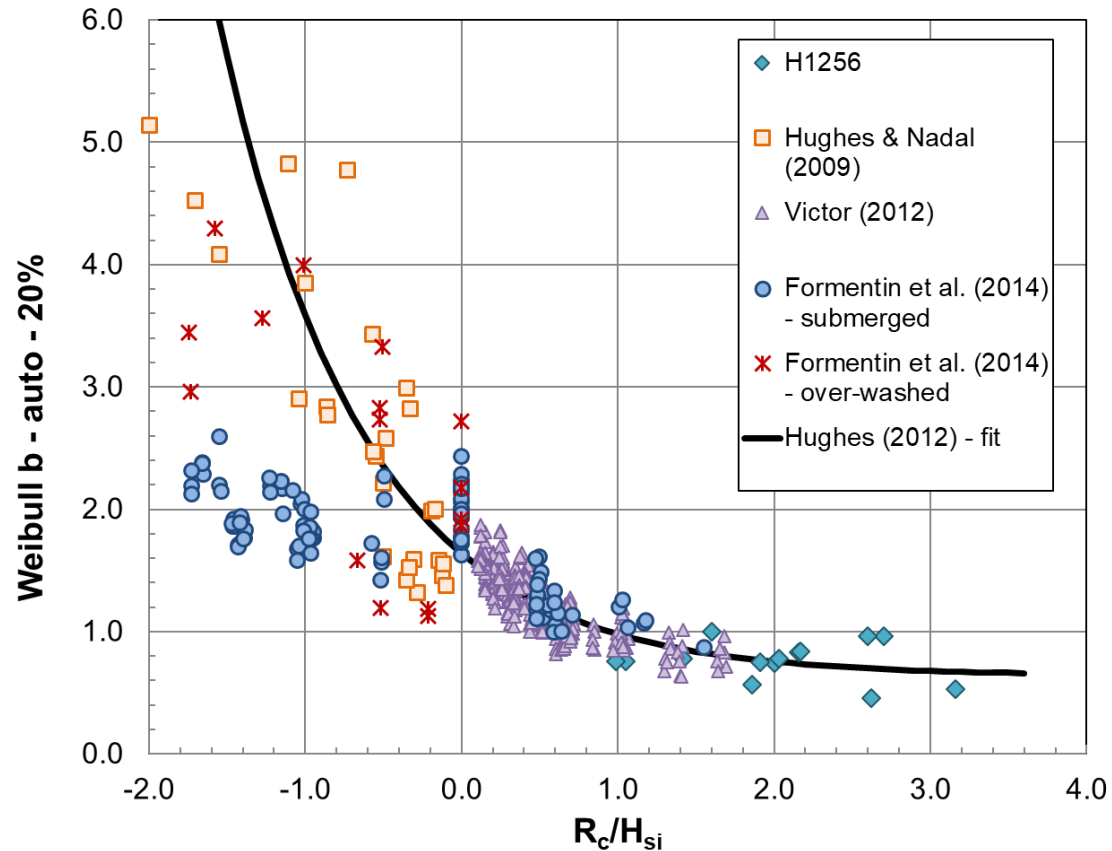
$$P(V_i \geq \bar{V}) = \exp\left(-\left(\frac{V}{a}\right)^b\right)$$



Applications: extreme overtopping volumes

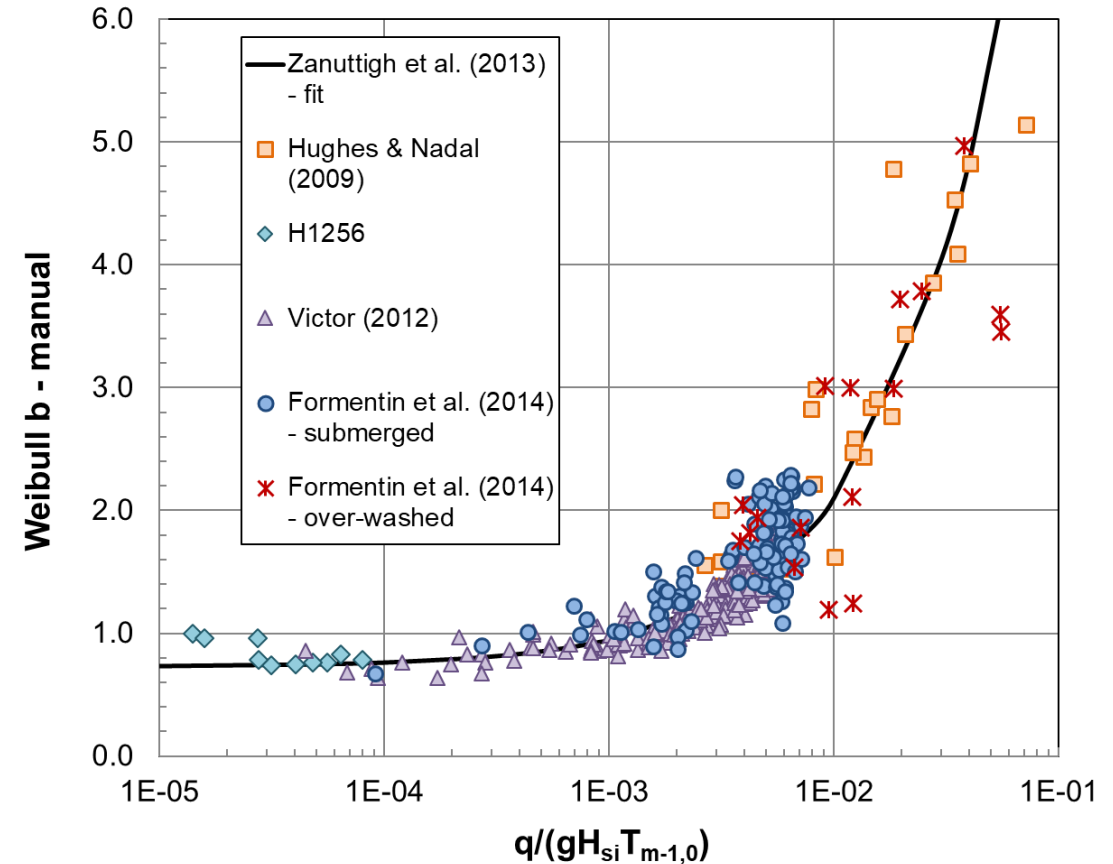
Hughes et al. (2012)

$$b = \left(\exp \left(-0.6 \frac{R_c}{H_s} \right) \right)^{1.8} + 0.64$$



Zanuttigh et al. (2013)

$$b = 0.73 + 55 \cdot \left(\frac{q}{gH_s T_{m-1,0}} \right)$$



Conclusions

- A new procedure has been developed for the **identification** and the **coupling** of the individual wave overtopping events
- The procedure is **fully automatic** and its accuracy is comparable to the accuracy of a manual analysis of the signals
- The procedure can process **any kind of oscillatory signal** in the time domain and can be applied to **any structure type** and **structure emergence**
- The wave identification algorithm can be applied to the processing of the discharge signals to reconstruct the distribution of the **overtopping volumes**
- The coupling algorithm allows the estimation of the **wave celerities** and the study of the evolution of the wave characteristics over the structure crest
- The main limit of the procedure is represented by the **sample frequency** of the input signals, i.e. a constraint independent of the procedure itself



References

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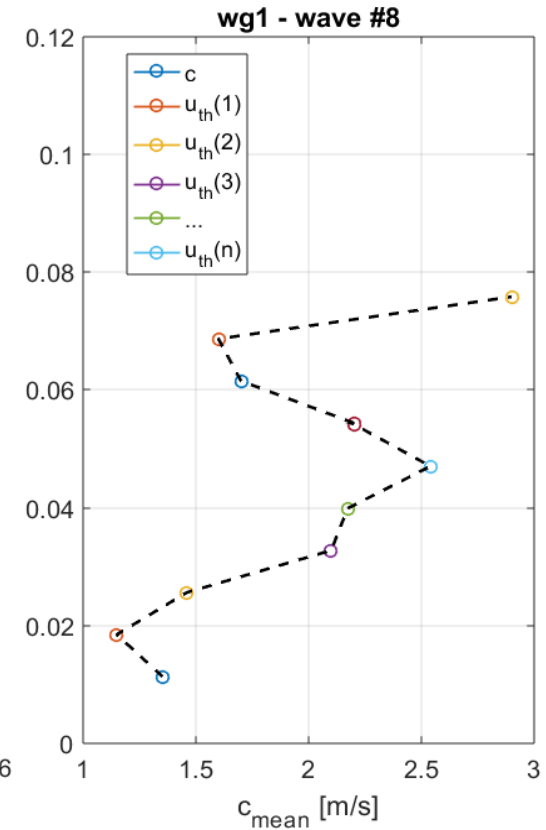
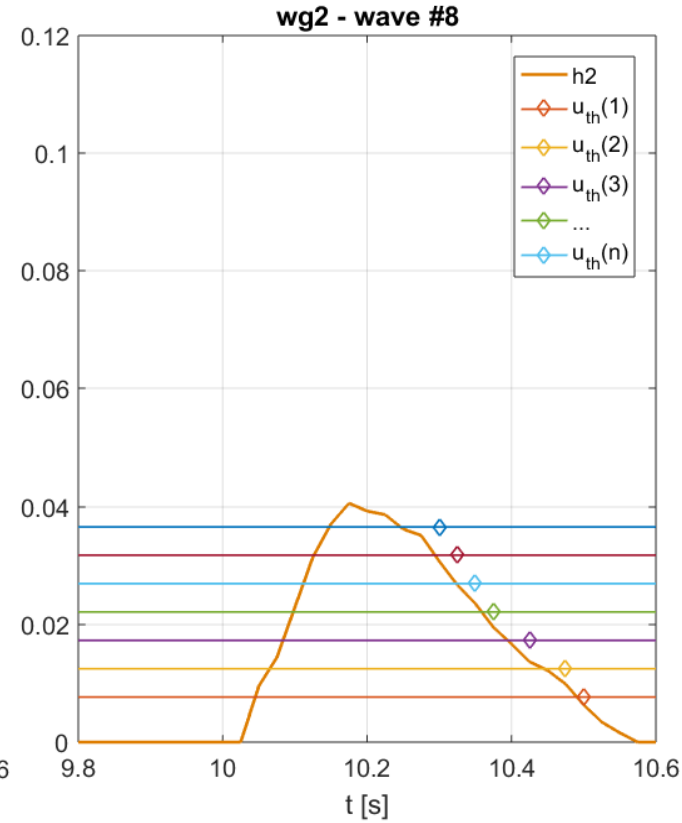
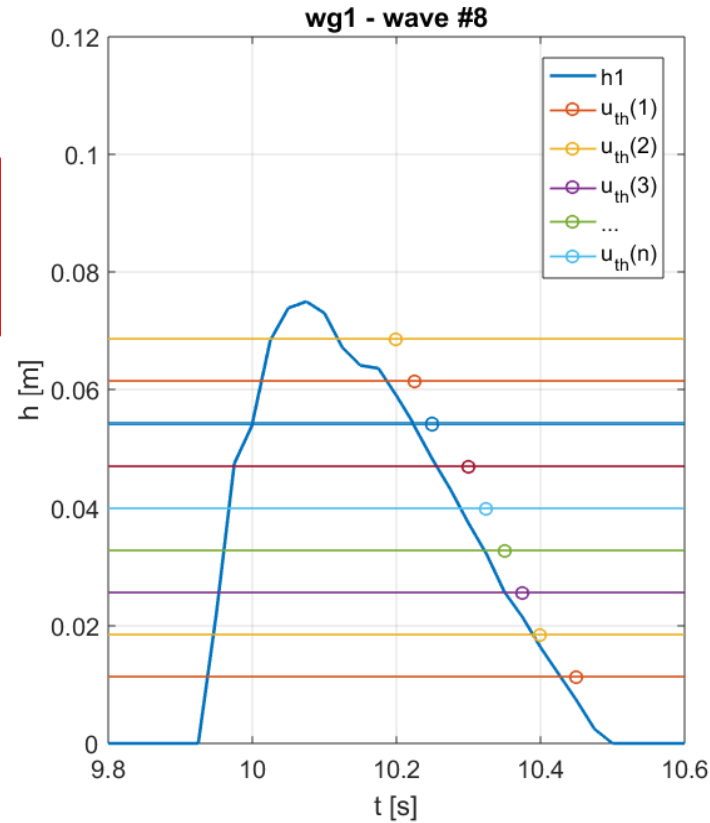


Wave coupling: the wave celerities

- For each i -th wave propagating from $wg1$ to $wg2$:

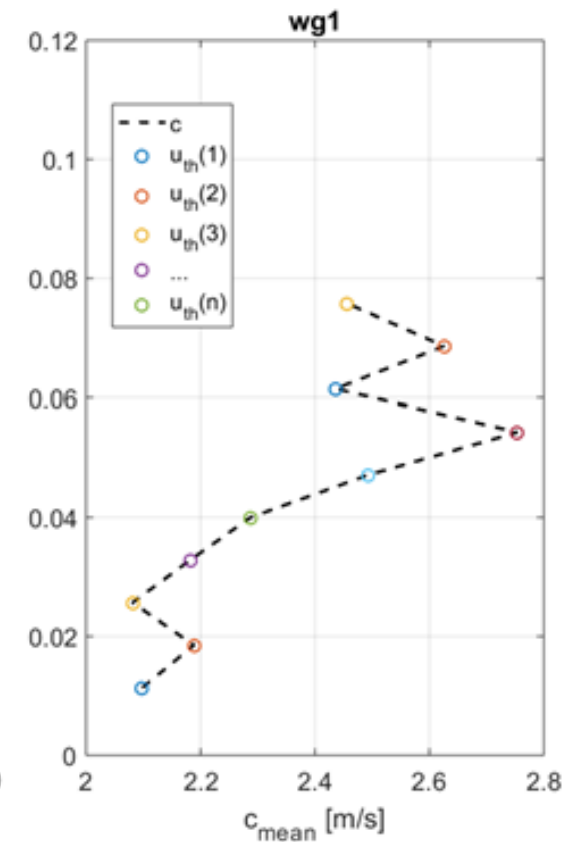
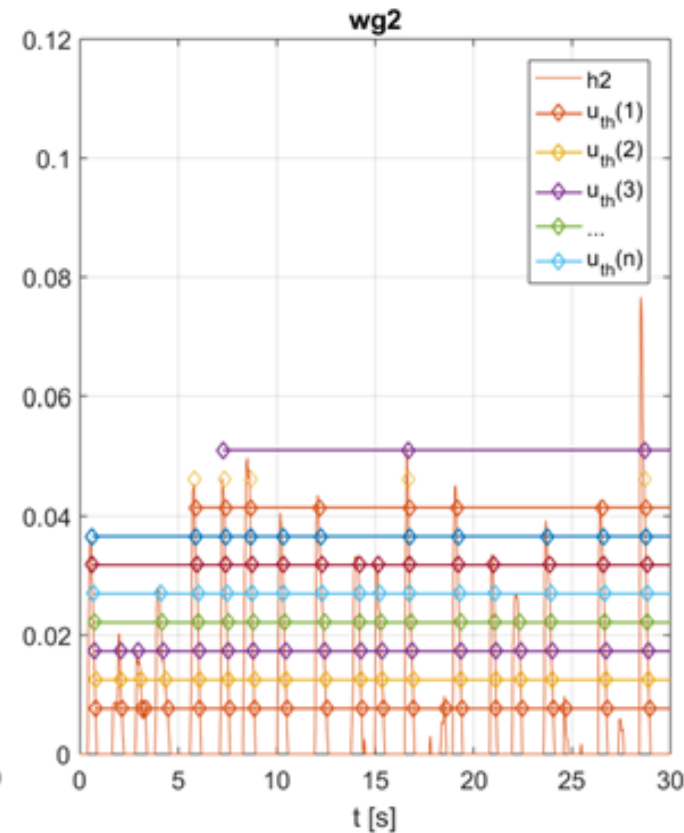
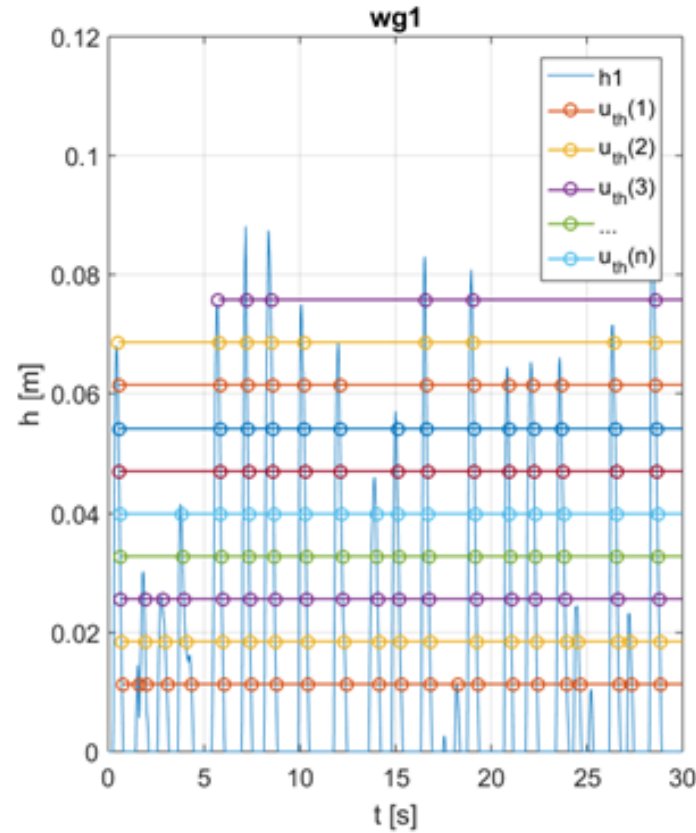
$$c(i) = \frac{diswg}{Dc2s(i) - Dc1s(i)}$$

- c can be computed at different elevations, reconstructing the **instantaneous vertical profile of c**



Wave coupling: the wave celerities

- Extraction of the **statistics** of the distribution of the c -values (mean, median, extreme quantiles, etc.)
- Reconstruction of the **vertical profile of mean c**



Applications: extreme overtopping volumes

		Hughes & Nadal (2009)	Experimental
$H_s/L_{m-1,0}$	0.02; 0.03; 0.04	0.02; 0.03; 0.04	0.03; 0.04
H_s [m]	2	2	0.8; 1.0; 1.2
h [m]	7.5; 8.5	7.5; 8.5	[5.2; 7]
R_c [m]	0; 0.5	0; 0.5	0; 0.5
R_c/H_s	-1.5; 1.5	-1.5; 1.5	[0.67; 1.8]
$\cot(\alpha_{off})$	2; 3; 4	2; 3; 4	2; 4
G_c [m]	3; 6; 9	3; 6; 9	3; 6
#	91	91	113

