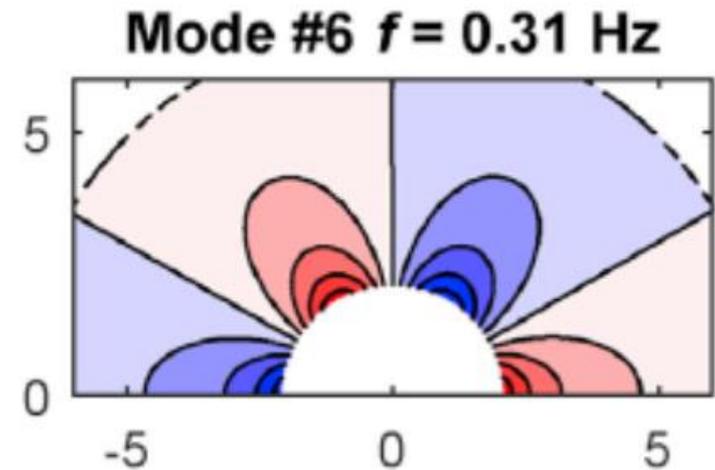


Empirical and numerical modal analysis of coastal areas prone to tsunami risk



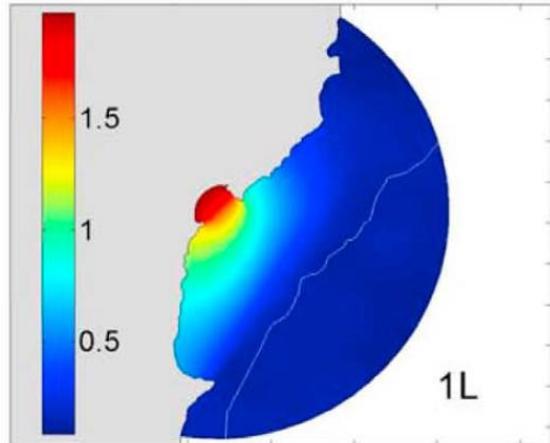
G. Bellotti¹, A. Romano²

¹ Roma Tre University, ² Sapienza Università di Roma

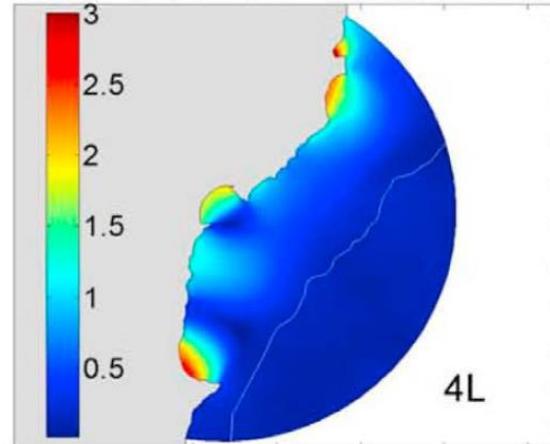
The importance of the modal response (natural modes) on tsunami amplification

- Shelf effects

$T=79.56$ min, $f=0.75$ c/h, $\zeta=3.07e-001$ h⁻¹

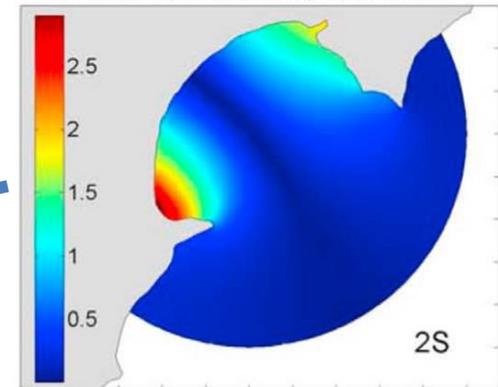


$T=41.67$ min, $f=1.44$ c/h, $\zeta=4.56e-001$ h⁻¹

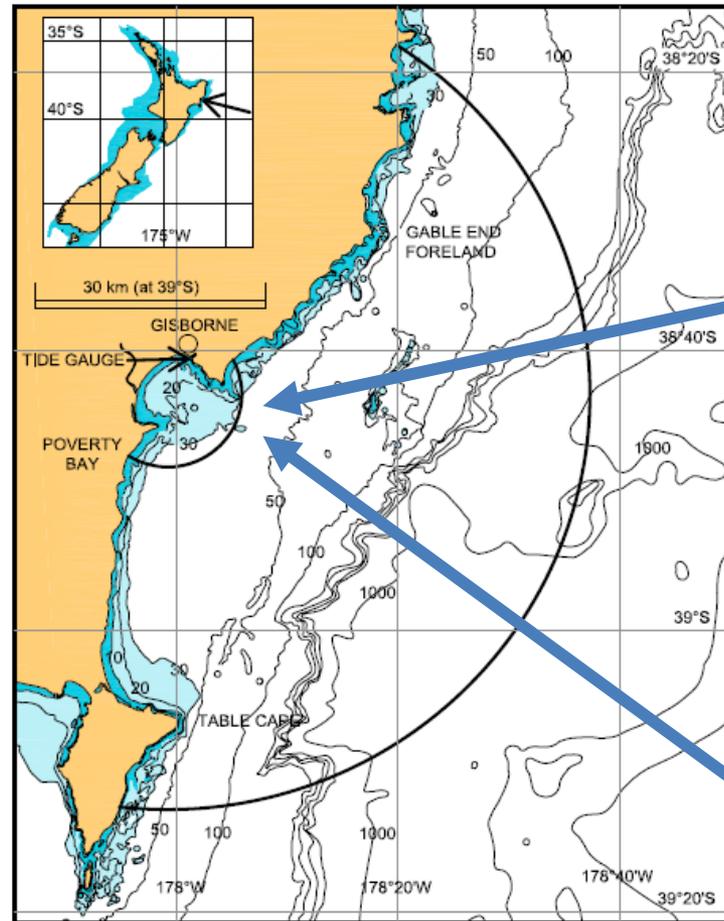
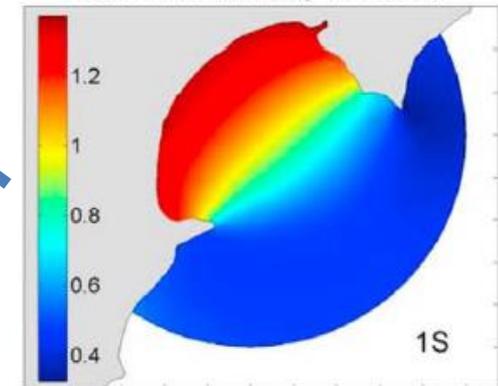


- Bay effects

$T=24.53$ min, $f=2.45$ c/h, $\zeta=1.32e-001$ h⁻¹



$T=50.03$ min, $f=1.20$ c/h, $\zeta=1.69e+000$ h⁻¹



Poverty Bay (NZ)

Edge waves generated by landslides?



Index of the presentation

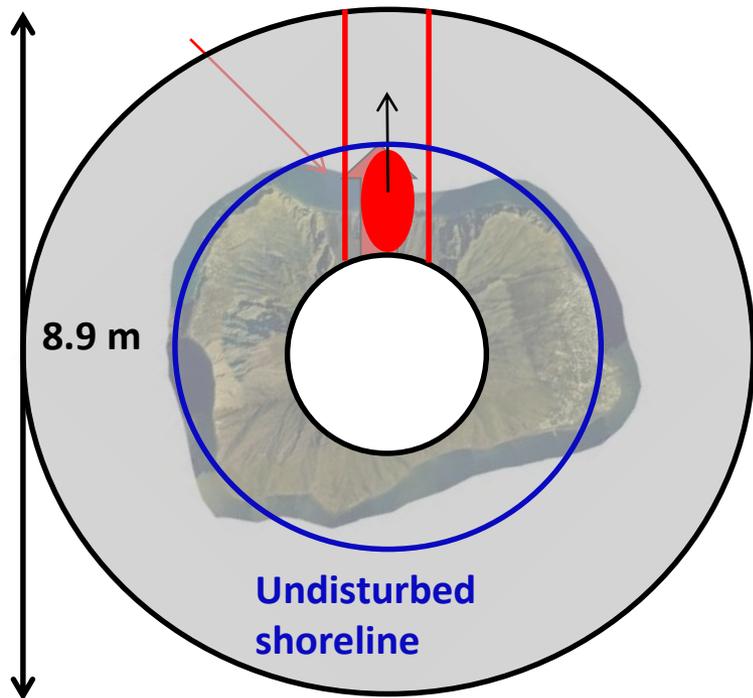
- Brief description of the experimental layout
 - Laboratory experiments with moveable wave gauges
- k-f analysis for the trapped waves
- EOF analysis for the trapped waves
- Numerical modal analysis



The conical island: a small simplified Stromboli

The physical model represents a truncated conical island (base radius 4.45 m). The slope of the island's flanks is 1:3 (1 vertical, 3 horizontal). A flat slope (0.5 m wide) allows the model to slide along the flank and to enter the water. The physical model roughly reproduces the small volcanic island Stromboli (South Tyrrhenian Sea, Italy) in a Froude law scale (1:1000).

Landslide model

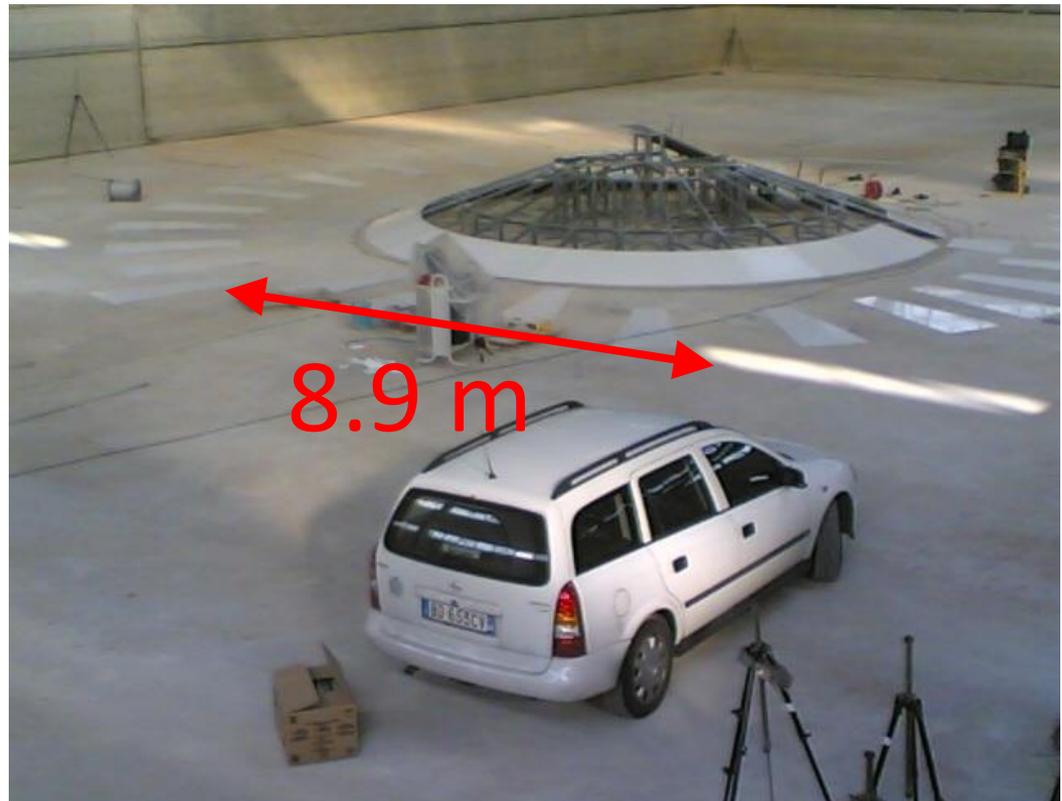


8.9 m

Undisturbed shoreline

Stromboli island

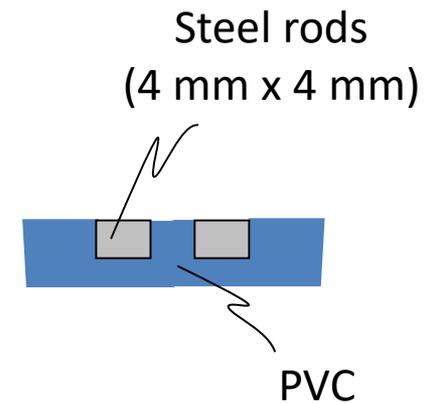
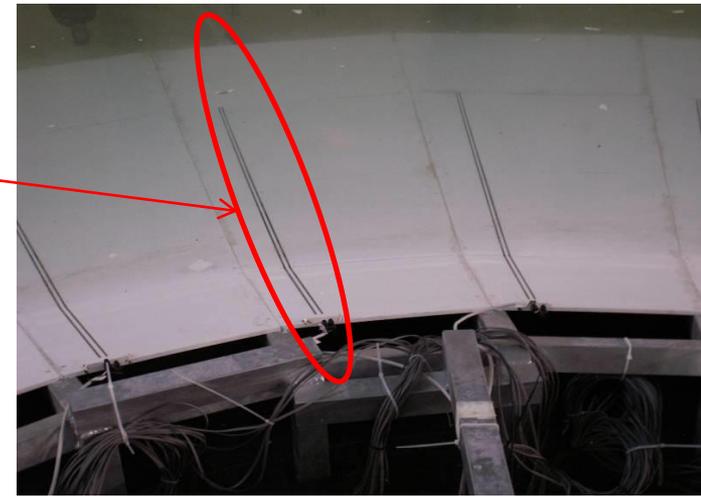
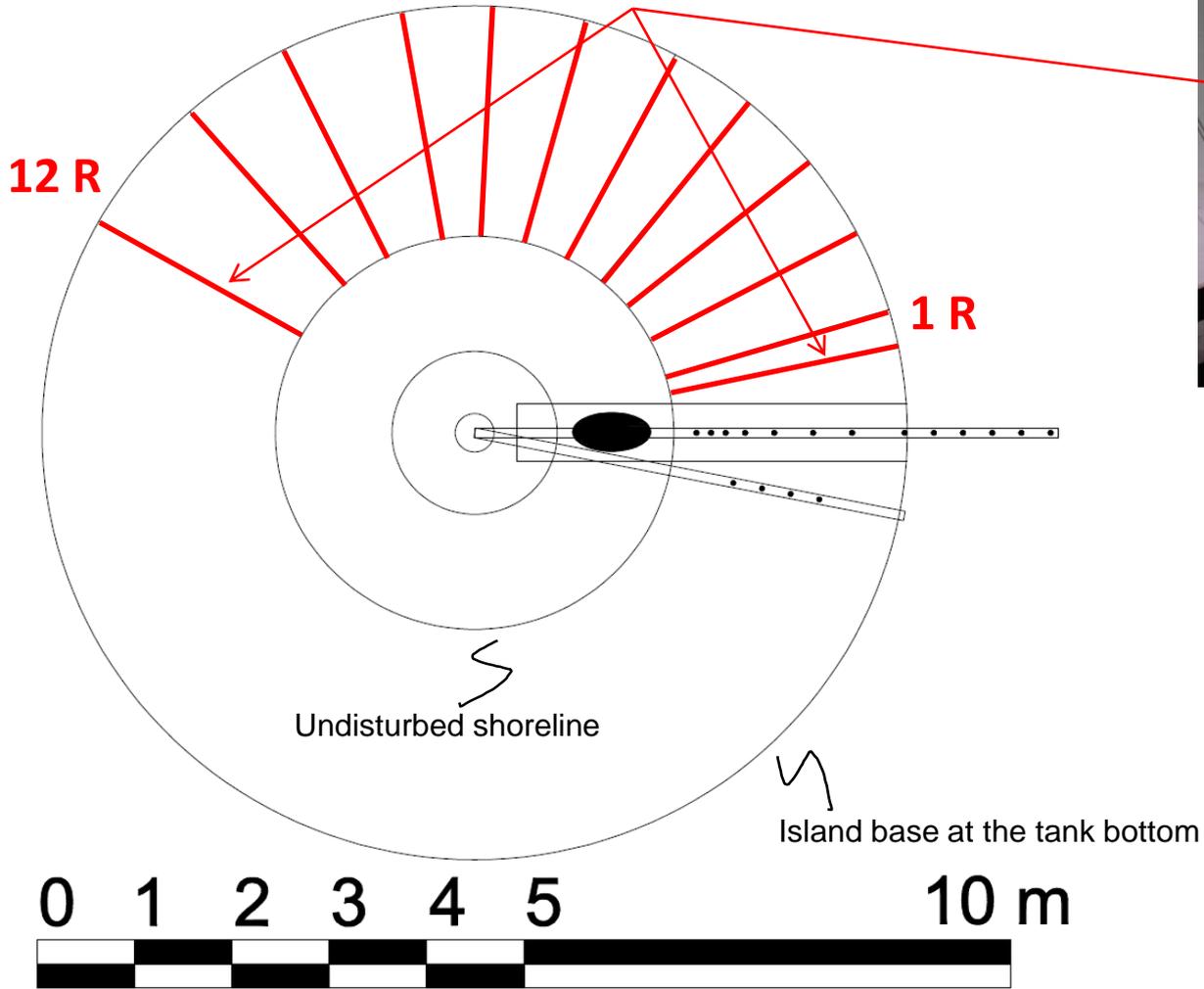
Technical University of Bari (Italy)



8.9 m

The run-up gauges

12 run-up gauges embedded in the PVC sheets



A movable arm to change the position of wave gauges

13 wave gauges are installed on a rotating arm, which is placed at the island center. An electric engine, remotely-controlled rotates it along an angular sector of **180°**, with steps of **5°**.



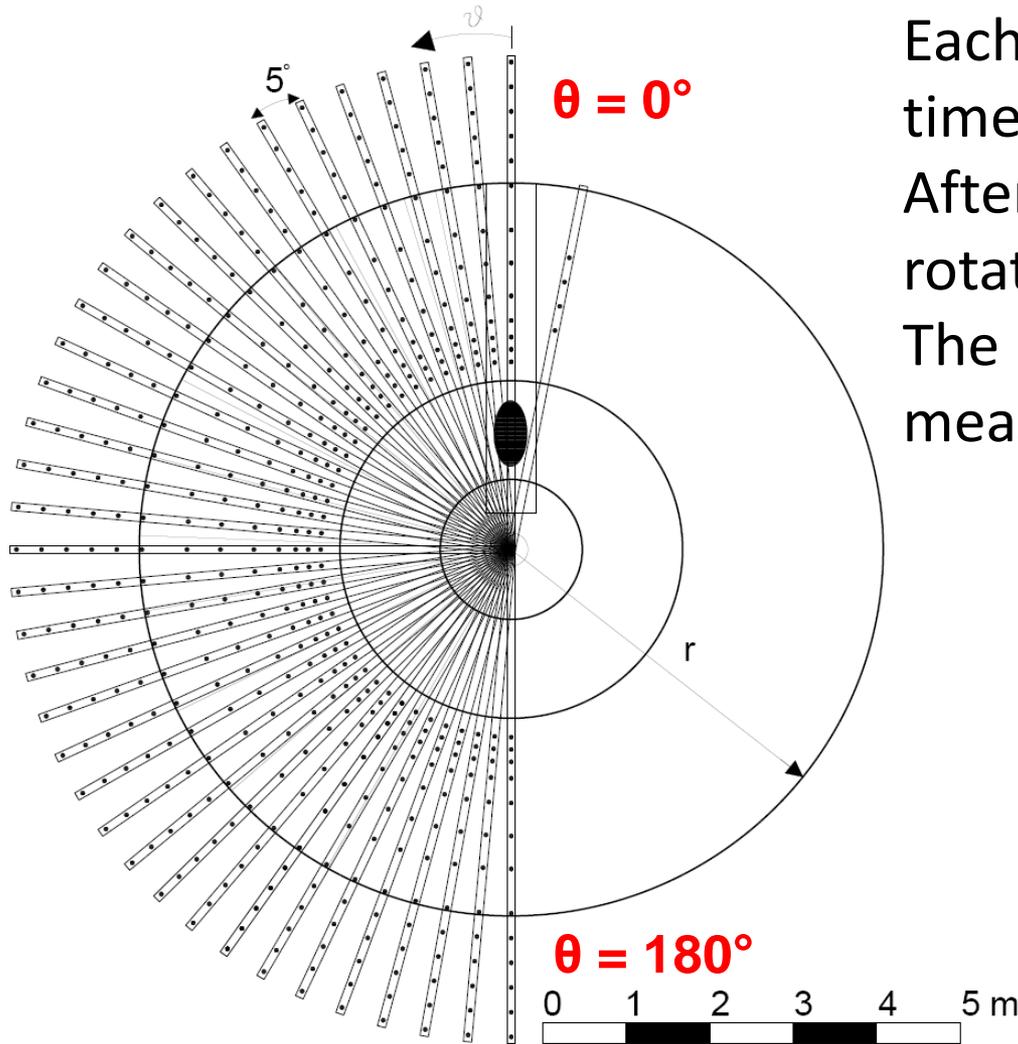
Electric engine remote-controlled

Rotating arm with instruments

0 1 2 3 4 5m

A scale bar with markings at 0, 1, 2, 3, 4, and 5 meters. The bar is black with white markings and is positioned below the technical drawing.

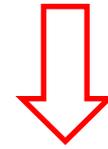
A movable arm to change the position of wave gauges



Each experiment is repeated 37 times.

After each test the arm has been rotated by 5° .

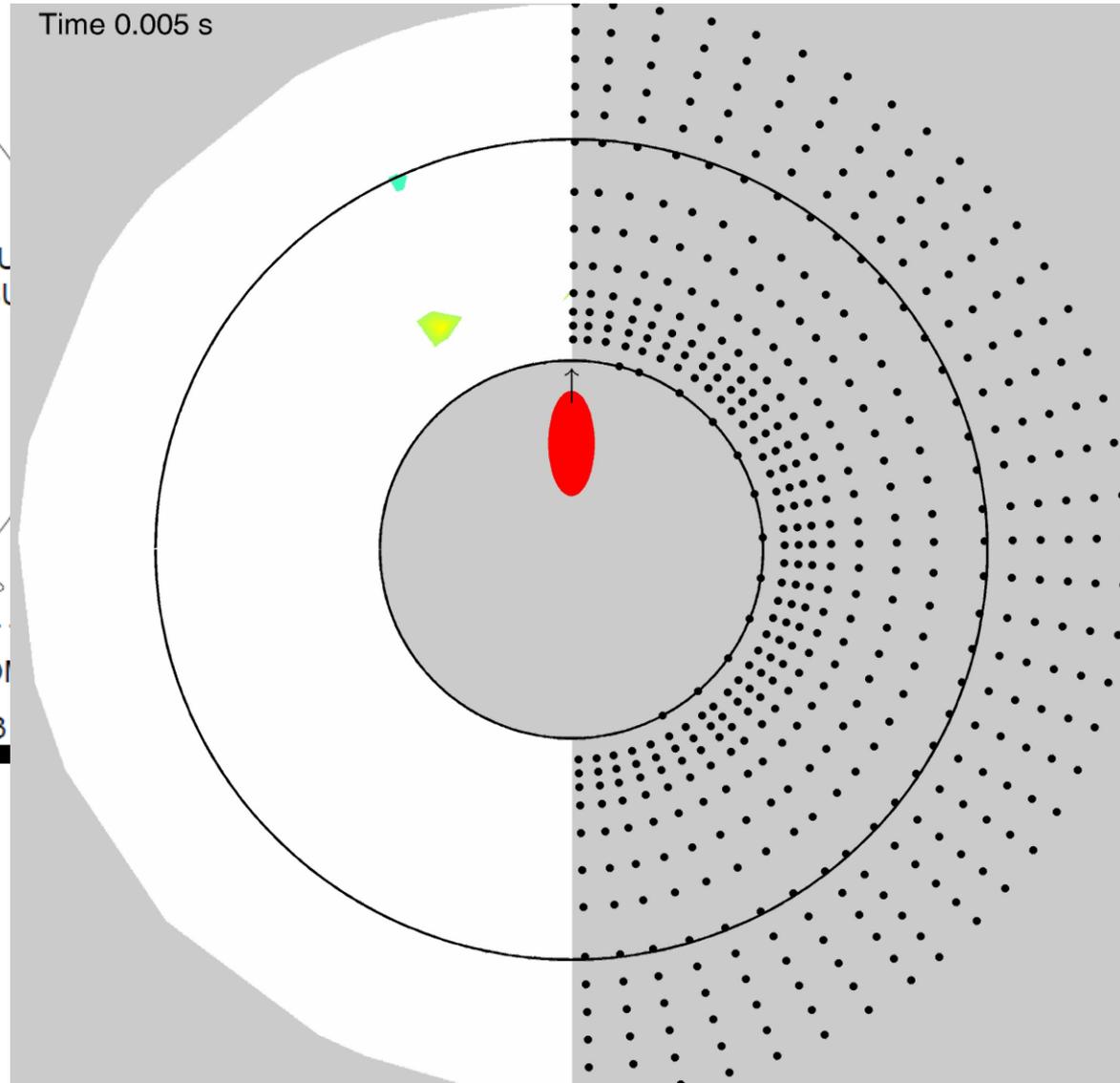
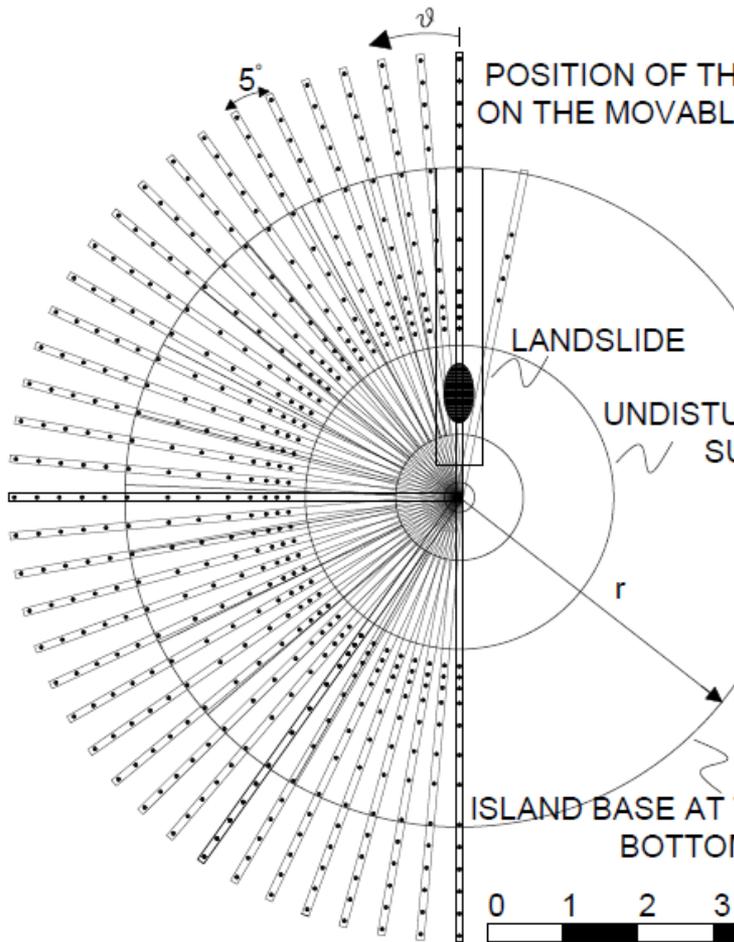
The arm position has been carefully measured by a theodolite.



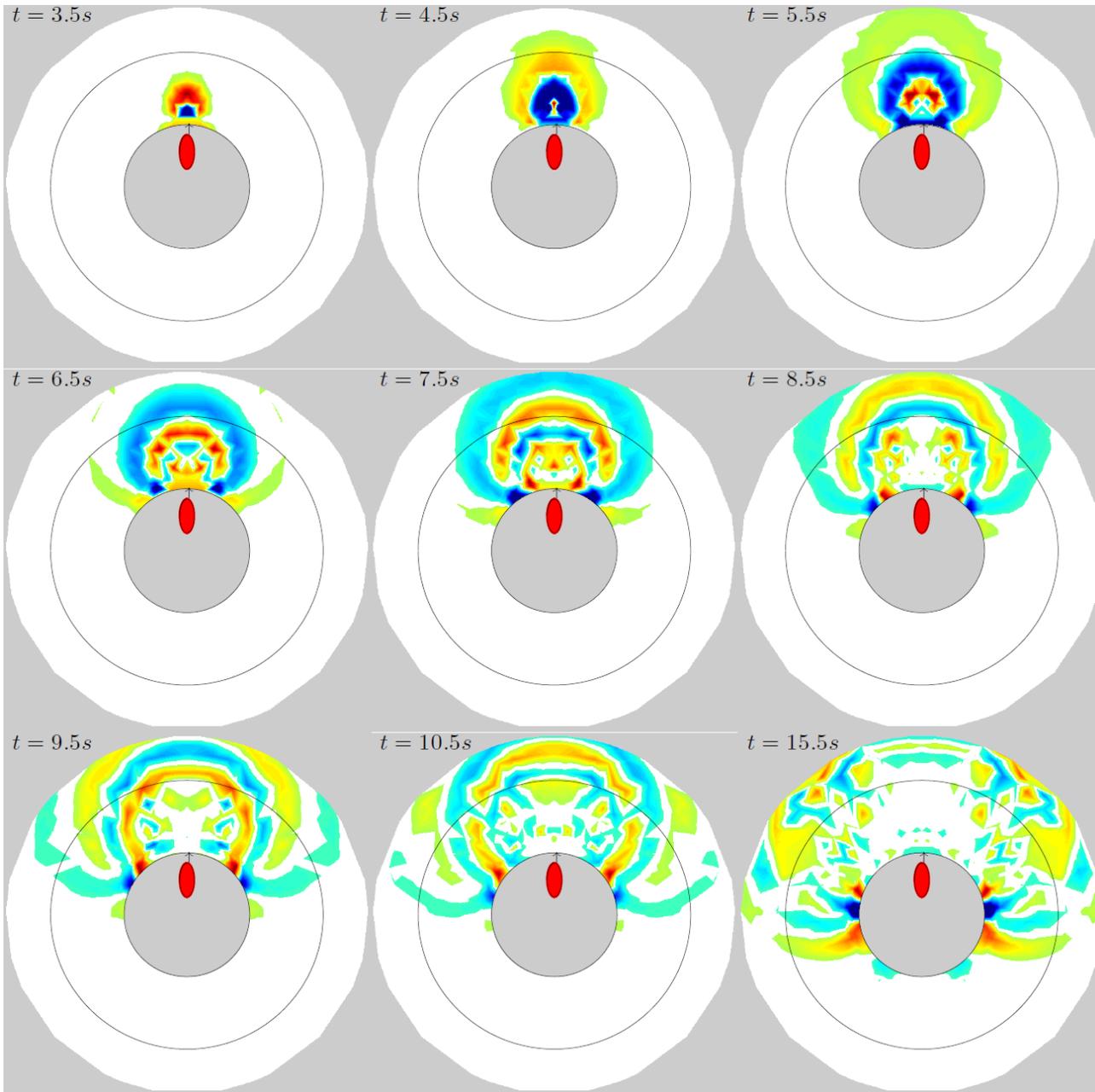
Once the repeatability of the experiments is ensured, more than **500** punctual free surface elevation time series are available

θ = Angle between the path of the landslide and the rotating arm

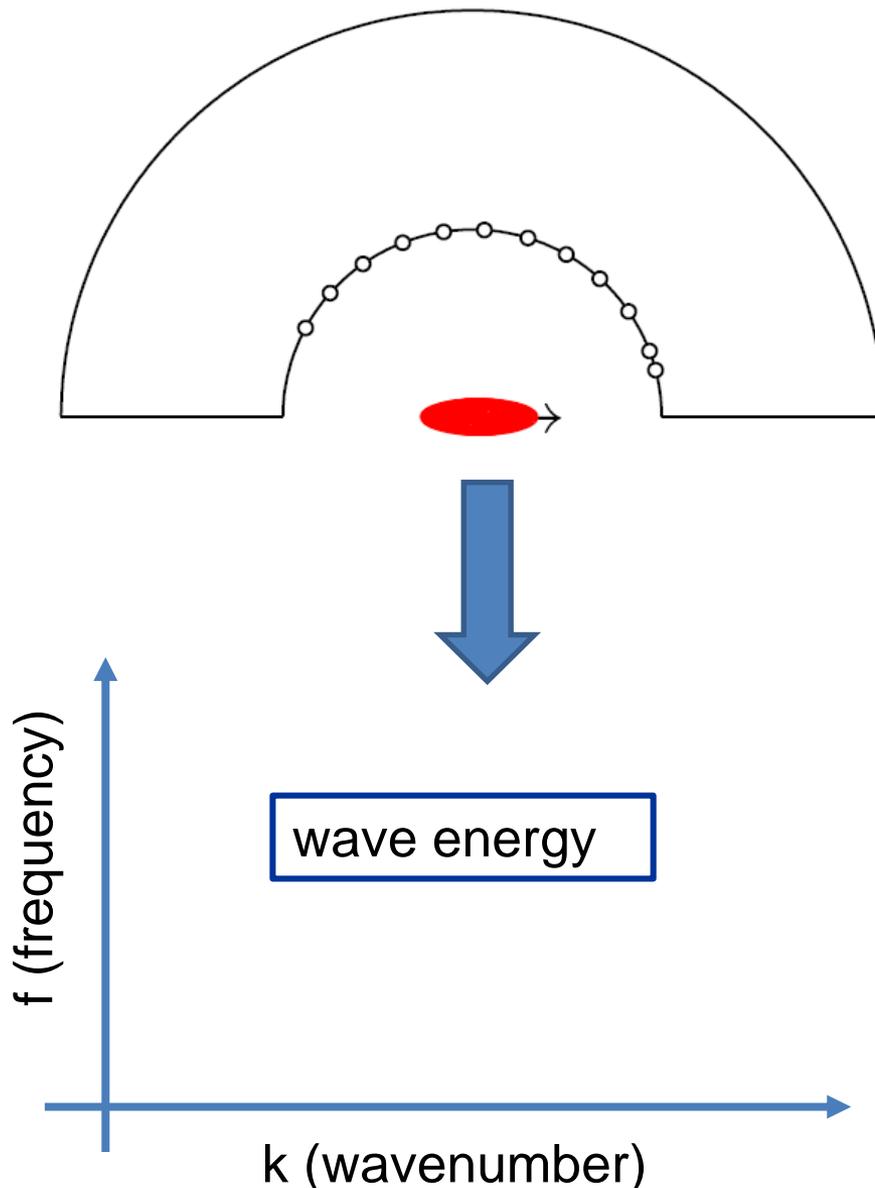
Animation of the results



Edge waves travelling around the island?



Wavenumber-frequency (k-f) analysis of the results



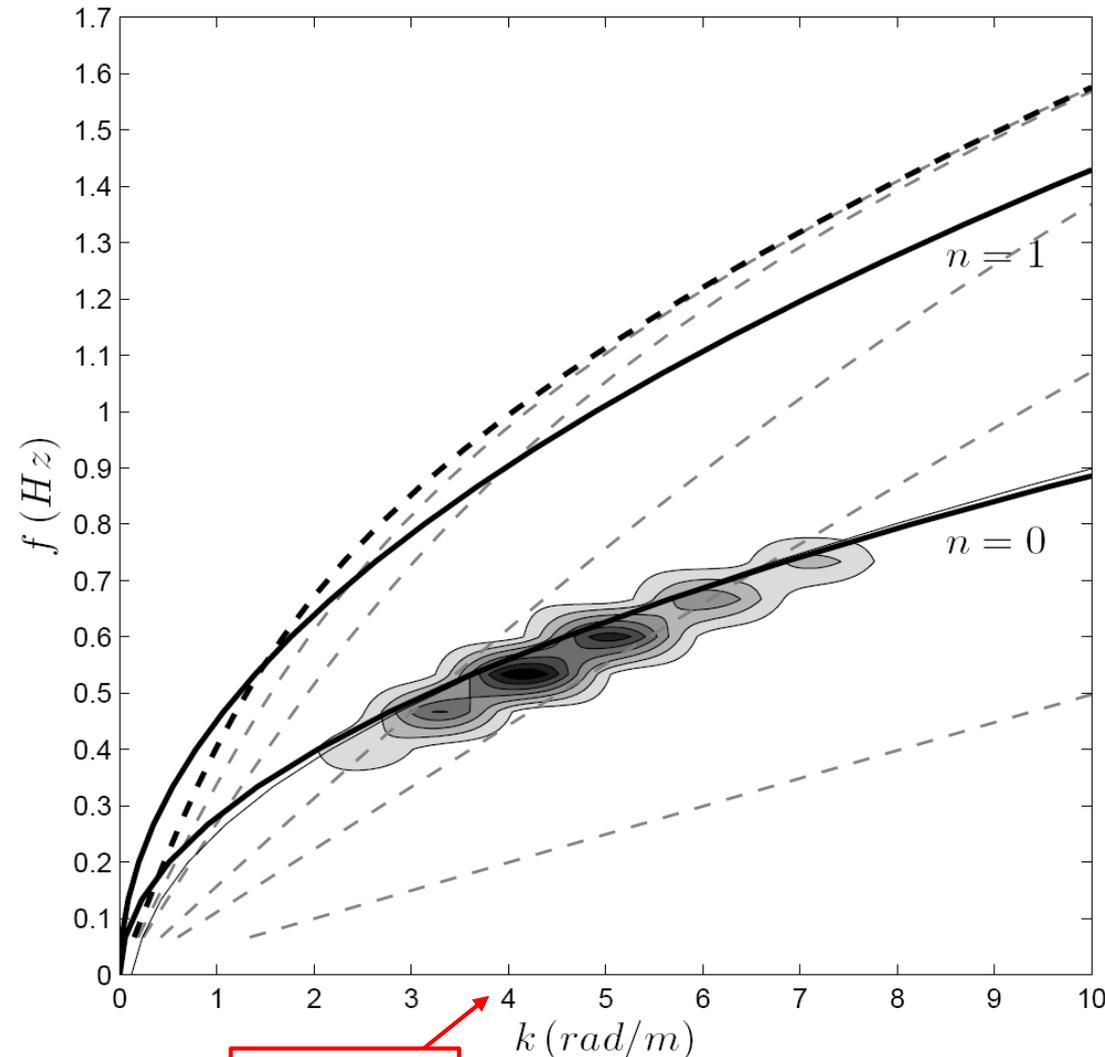
The run-up time series are processed to obtain

The wave energy distribution in the k-f domain

Romano A., Bellotti G., Di Risio M. (2013). Wavenumber-frequency analysis of the landslide-generated tsunamis at a conical island. Coastal Engineering, vol. 81, pp. 32-43.

Wavenumber-frequency (k-f) analysis of the results

The 1D k-f, applied to the run-up time series, shows that the waves propagate along the shore as a **0th-order edge waves packet** or Stokes edge waves (*Ursell, 1952*).



L=1.5 m

Dispersion relationships:

- Deep water limit
- Edge waves ($n = 0, 1$)
- Edge waves (circular shoreline)
- · - Small amplitude waves

Edge waves (*Ursell, 1952*)

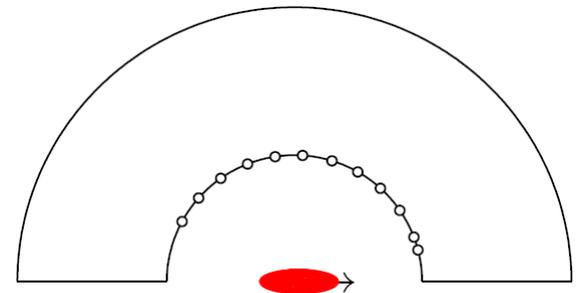
$$\omega^2 = g k \sin [(2n + 1) \beta]$$

Edge waves (circular shoreline, *Smith & Sprinks, 1975*)

$$\omega^2 = g k \tan \beta \left[1 - \frac{1}{4} (k r_s)^{-1} \right]^2$$

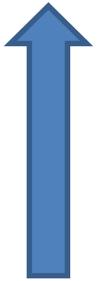
Small amplitude waves

$$\omega^2 = g k \tanh (k h)$$



The empirical orthogonal function method

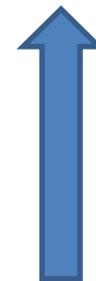
$$\eta(x, y, t) = \sum_{n=1}^N \alpha_n(t) \Gamma_n(x, y)$$



Surface
elevation



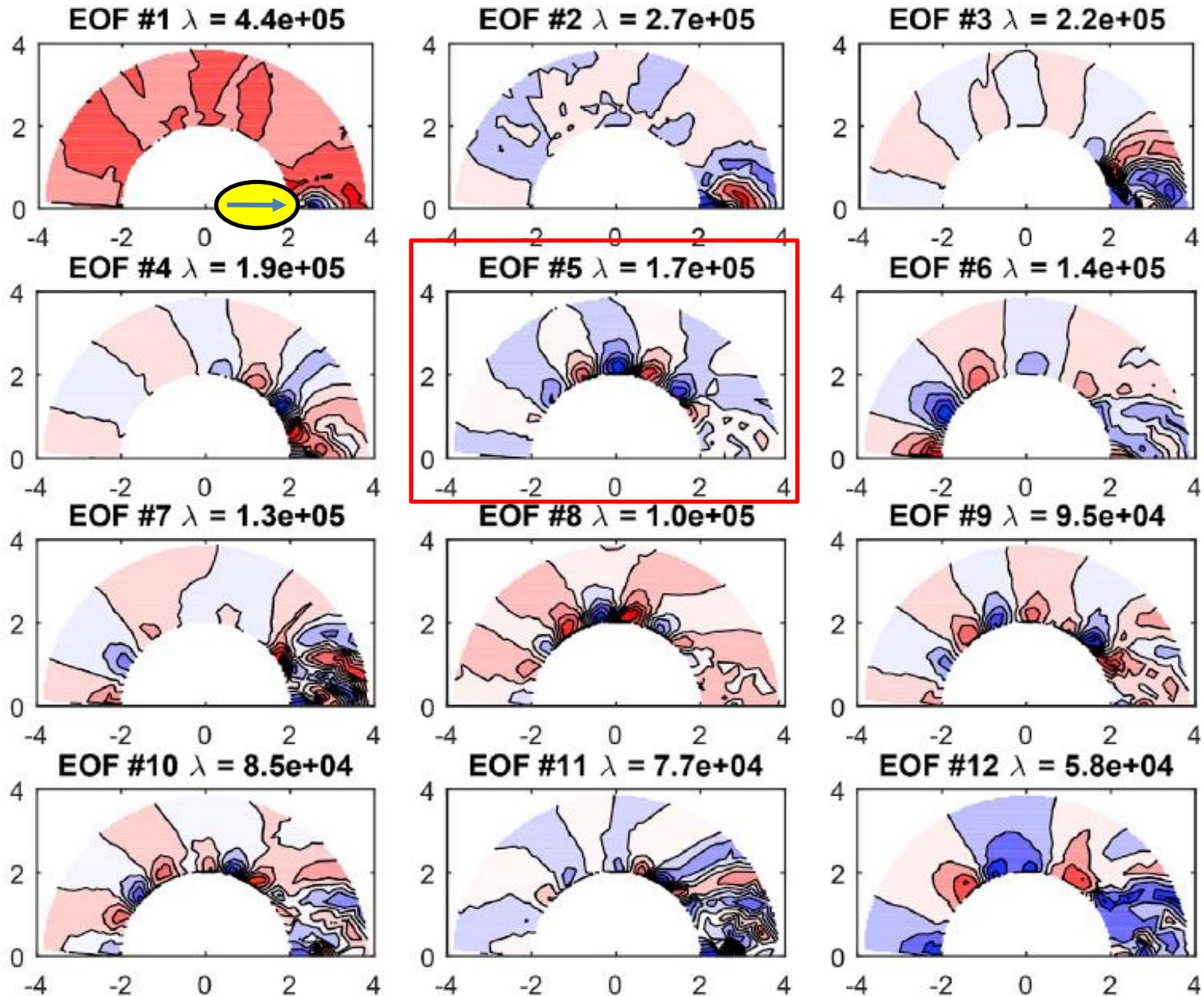
Time
function of
the n^{th} mode



n^{th} spatial
mode

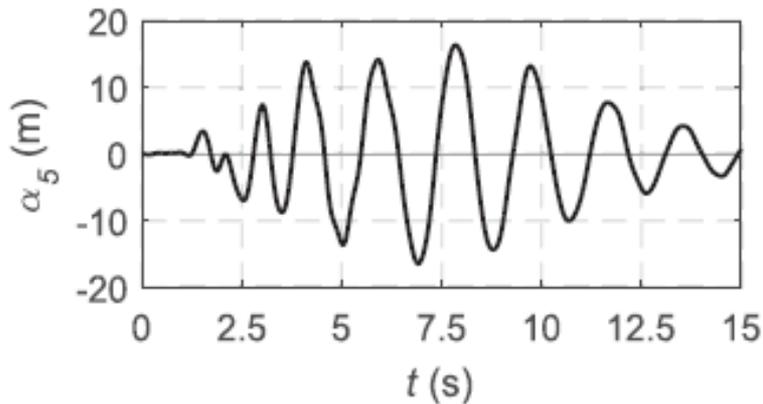
It is possible to calculate the amount of variance λ_n explained by each mode

The spatial modes calculated by the EOF method

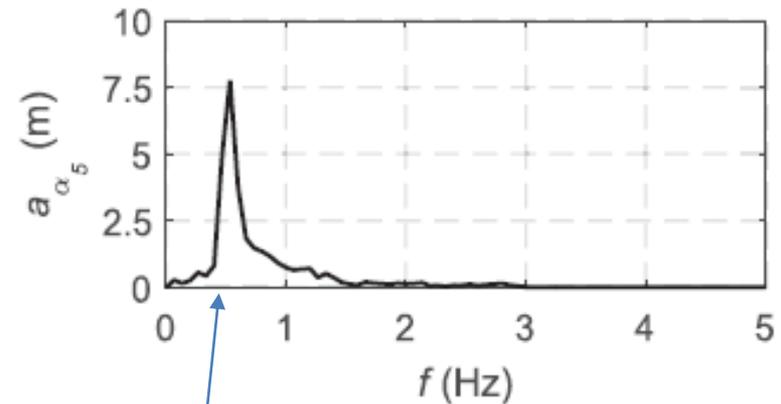


Further processing the EOF modes

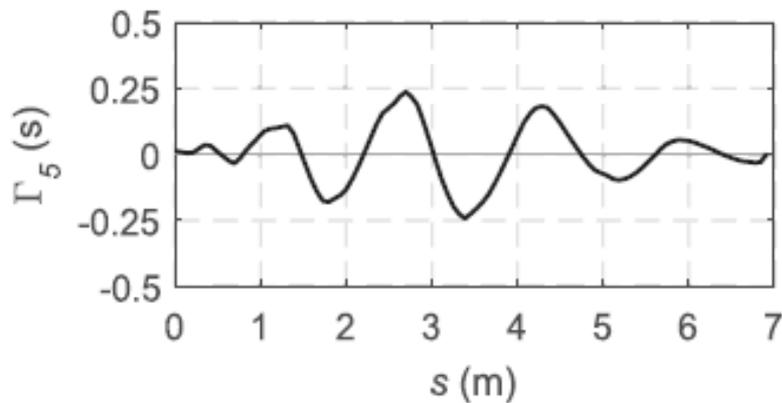
Time function for the mode $n=5$



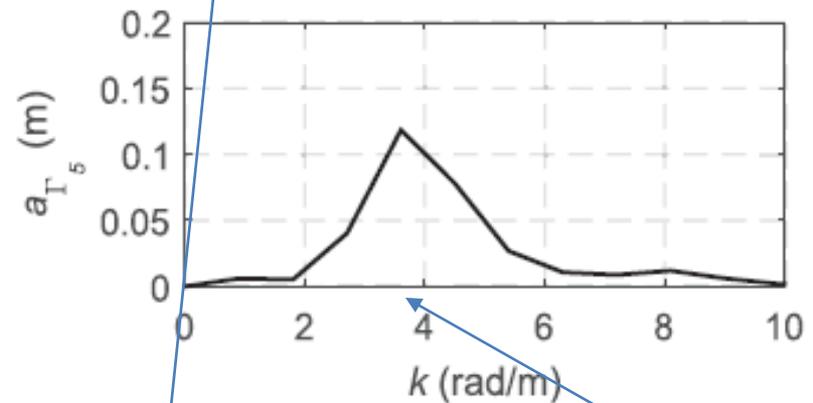
Frequency spectrum



Spatial mode elevation along the shoreline

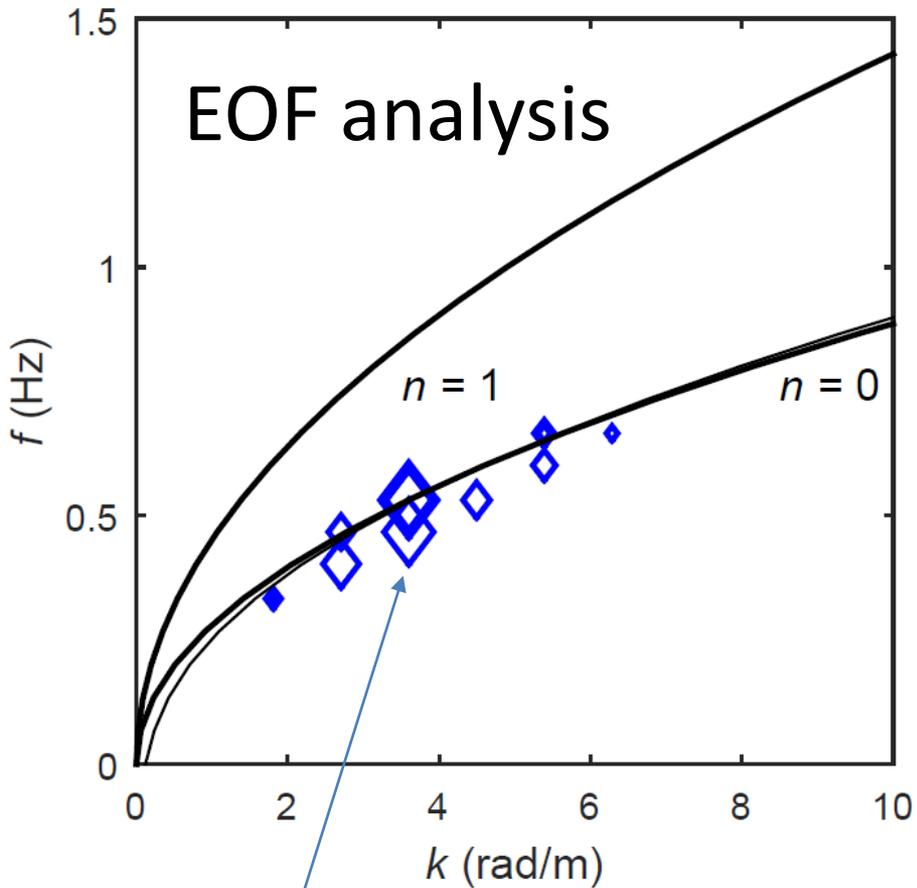


Wavenumber spectrum

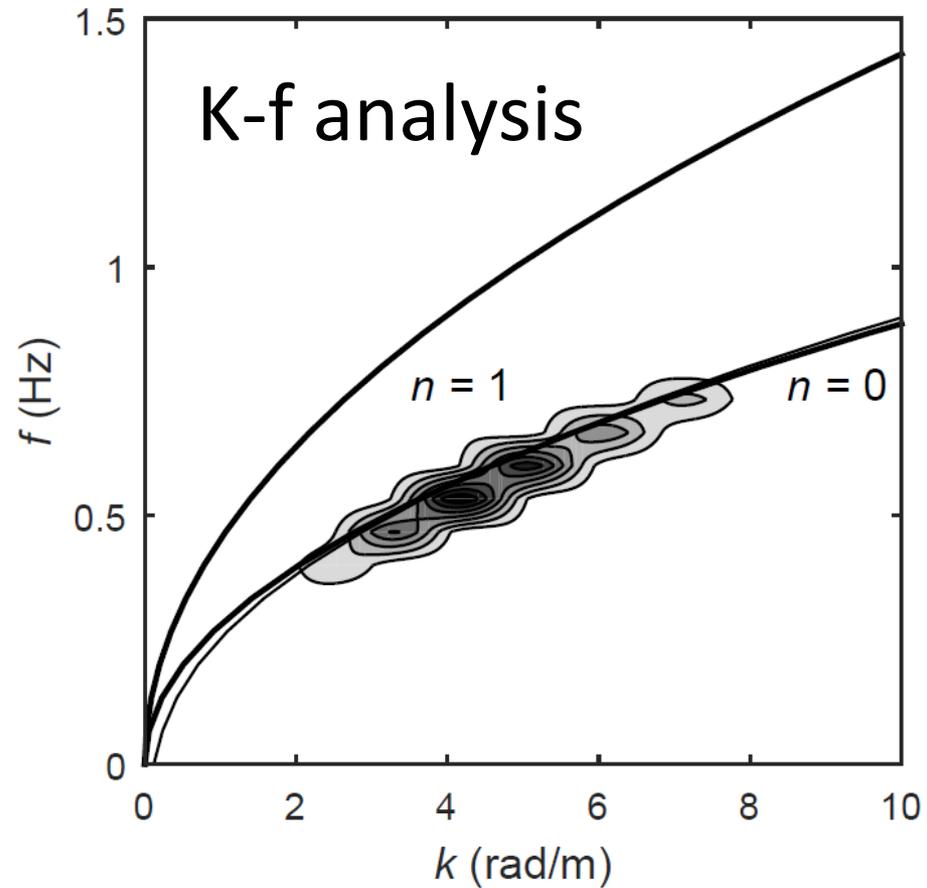


Each EOF mode can be associated to one peak frequency and one peak wavenumber

EOF and k-f results



Each EOF mode is represented by a marker
The size of the marker scales with λ_n



Dispersion relationships:

- Edge waves ($n = 0, 1$)
- Edge waves (circular shoreline)

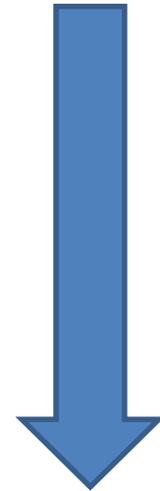
Numerical modal analysis

$\eta=0$, at $r=r_0$
Artificial open
boundary

shoreline

$\eta_n=0$, at $r=r_s$

$$\eta_{tt} - \nabla(gh\nabla\eta) = 0$$
$$\eta = \text{Re}[X(x, y)e^{-i\omega t}]$$

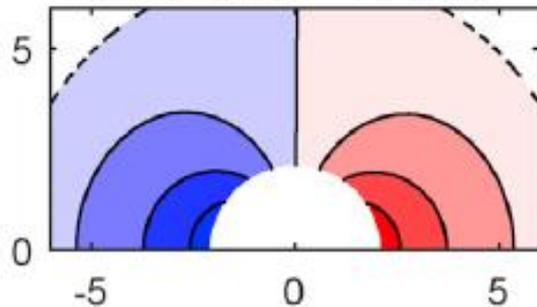


$$\omega^2 X - \nabla(gh\nabla X) = 0$$

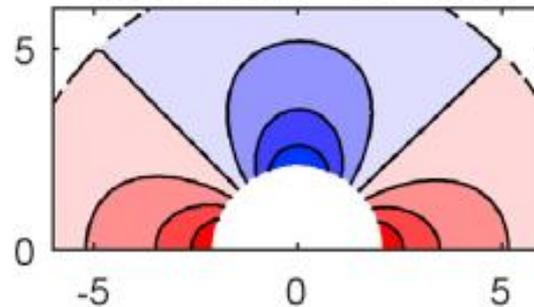
Eigenvalue problem

Numerical modal analysis results

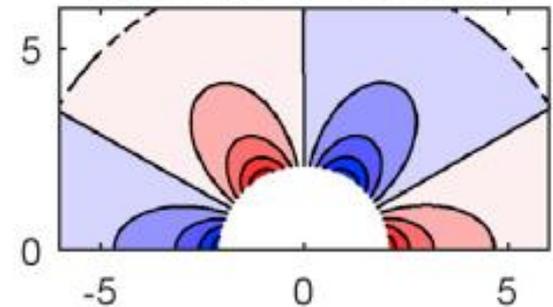
Mode #2 $f = 0.19$ Hz



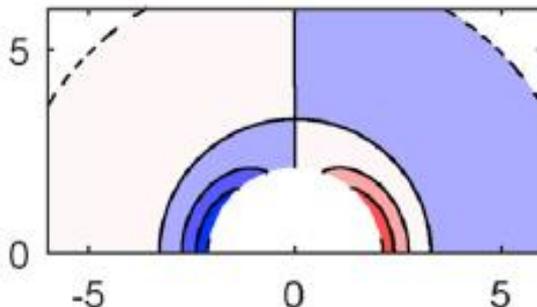
Mode #4 $f = 0.24$ Hz



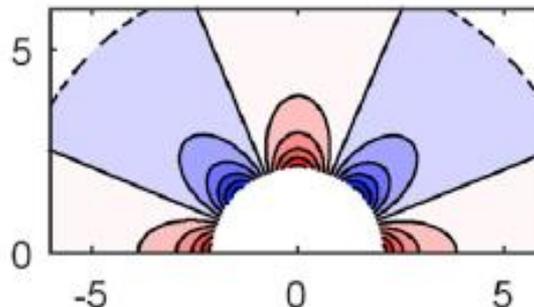
Mode #6 $f = 0.31$ Hz



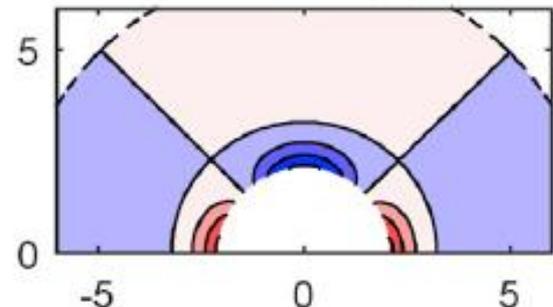
Mode #9 $f = 0.36$ Hz



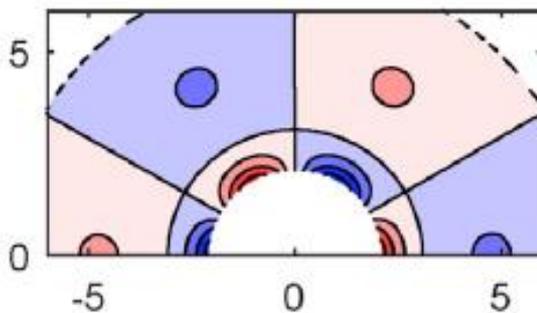
Mode #11 $f = 0.37$ Hz



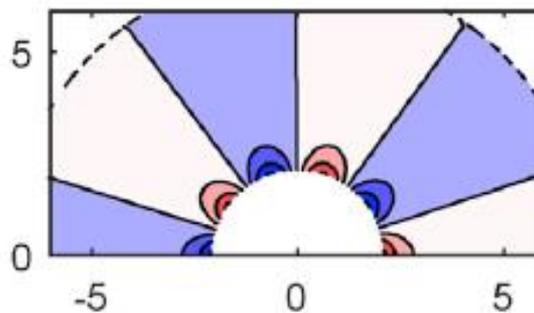
Mode #13 $f = 0.38$ Hz



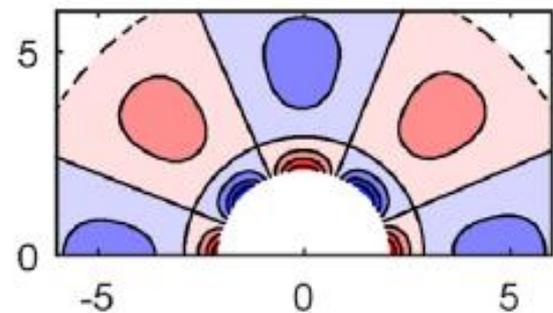
Mode #15 $f = 0.42$ Hz



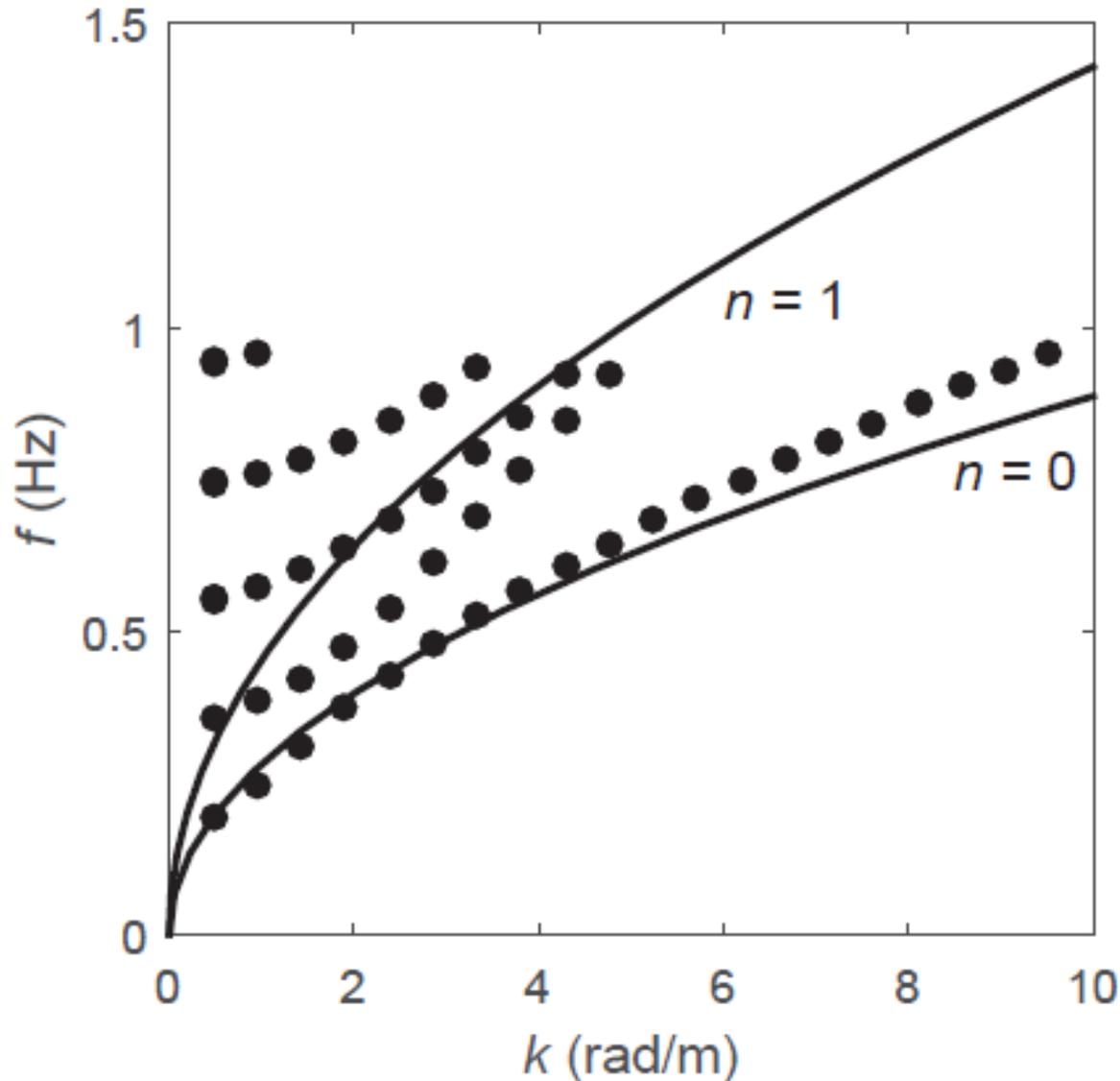
Mode #18 $f = 0.43$ Hz



Mode #19 $f = 0.47$ Hz

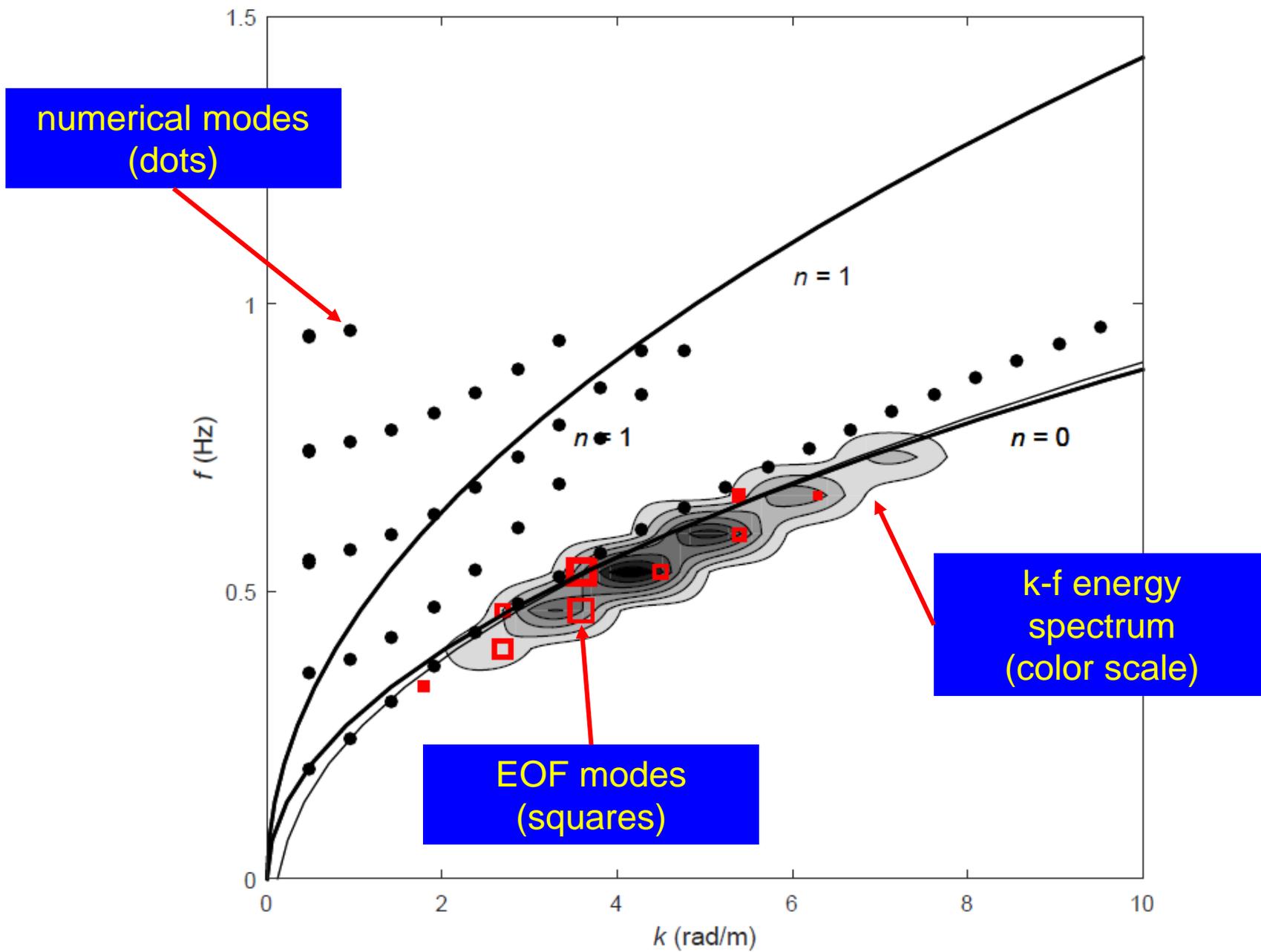


Numerical modal analysis results processed and plotted in the k-f plane



Each numerical mode is represented by a point. Here no information on the size/importance of the modes as the model simulates free (unforced) oscillations

Comparison of the methods



Conclusions

- Three methods for modal identification applied to experimental landslide tsunamis:
 - K-f spectral analysis, non information on the spatial shape of the modes
 - EOF spatial shape, k , f and relative importance (i.e. variance explained)
 - Numerical modal analysis: free response, no information on the importance of the modes
- Results in good agreement
- Edge waves (zeroth mode) dominate the wave propagation around the island

References

Movable arm experiments:

Romano A., M. Di Risio, G. Bellotti, M. G. Molfetta, L. Damiani, P. De Girolamo (2016). Tsunamis generated by landslides at the coast of conical islands: experimental benchmark dataset for mathematical model validation. *Landslides*, pp. 1-15.

Benchmark data available

k-f analysis:

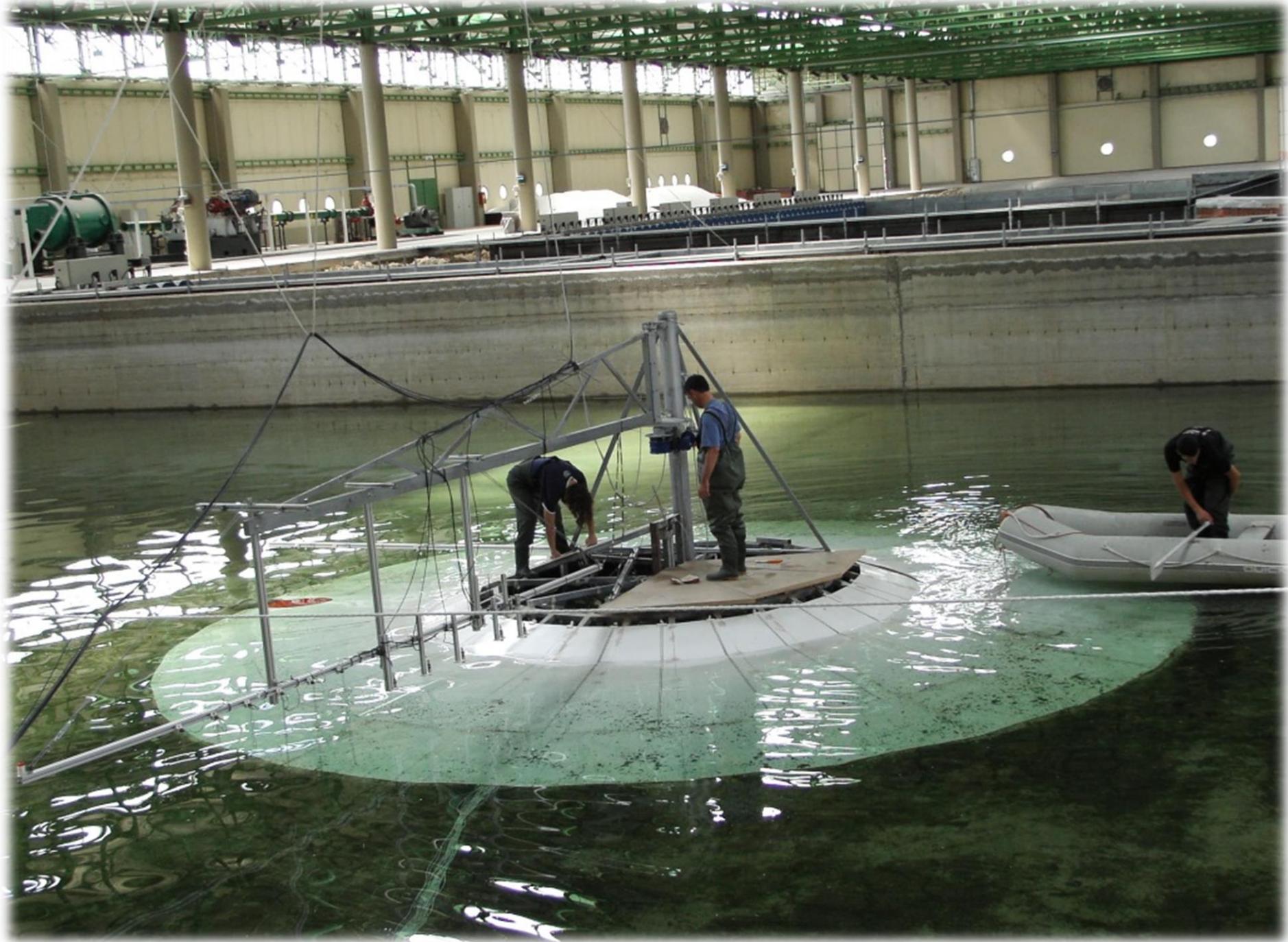
Romano A., Bellotti G., Di Risio M. (2013). Wavenumber–frequency analysis of the landslide-generated tsunamis at a conical island. *Coastal Engineering*, vol. 81, pp. 32-43.

EOF analysis:

Bellotti G., Romano A. (2017). Wavenumber-frequency analysis of landslide-generated tsunamis at a conical island. Part II: EOF and modal analysis. *Coastal Engineering*, vol. 128, pp. 84-91.

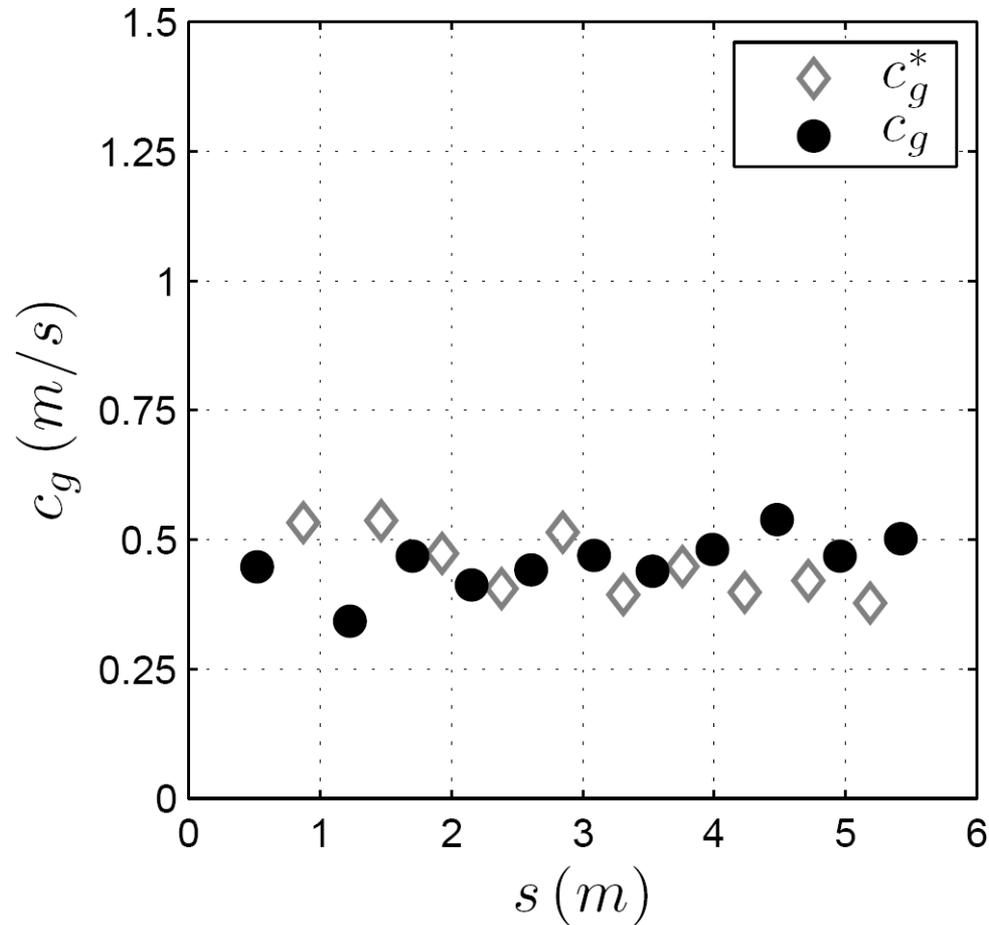
Submerged landslides:

Tsunamis generated by submerged landslides at a conical island: experimental and numerical analysis (in preparation)



Estimate of the wave group celerity

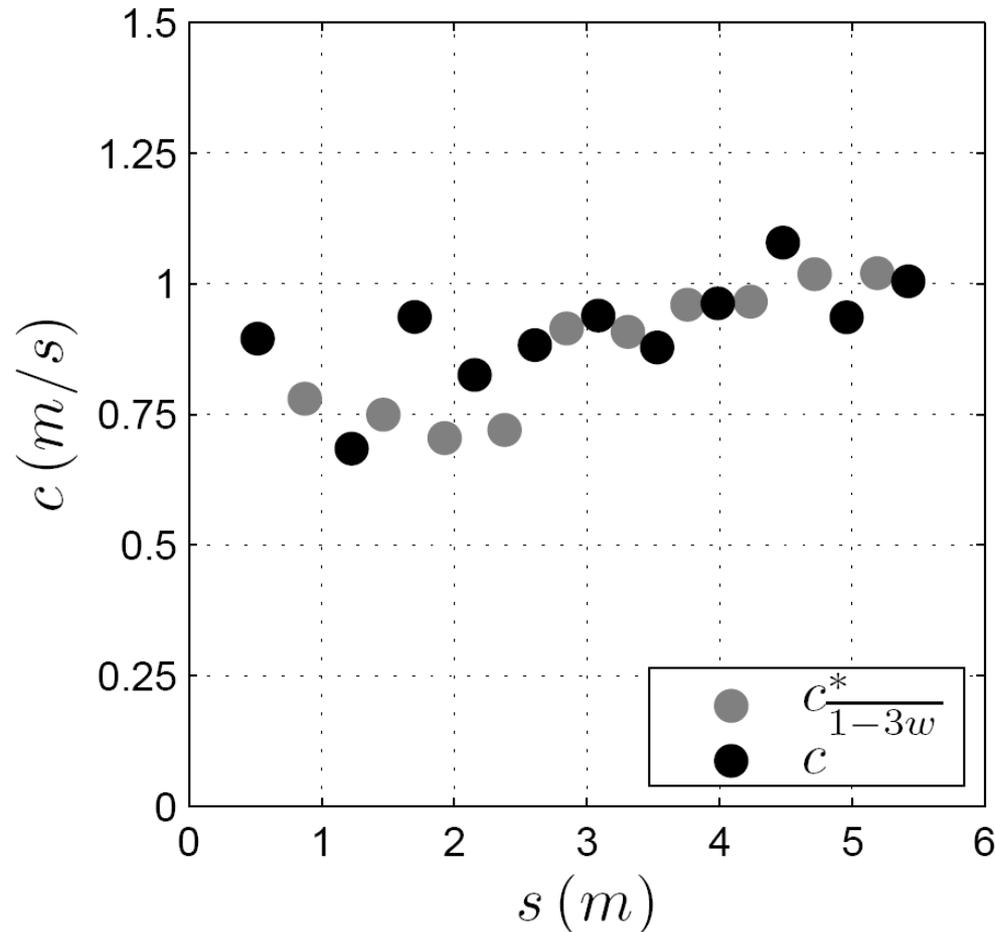
The theoretical group wave celerity, as from the edge waves theory for the 0-th mode, is in very good agreement with the experimental one.



$$s = r \theta$$

Estimate of the wave phase celerity

The experimental phase wave celerity of the first three waves that form the packet (c_{1w}^* , c_{2w}^* , c_{3w}^*) has been calculated as from the zero-crossing analysis, while the theoretical one has been obtained (c) by the edge waves dispersion relation.



$$s = r \theta$$

represents the distance from the impact point, measured along the shoreline