AGED ASPHALTIC REVETMENTS ON (SATURATED) SAND TESTED IN A LARGE DELTAFLUME

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Content



- Introduction
- Physical model tests
- Analysis of test results
- Conclusions and recommendations

2. Physical model tests



- Delta Flume Deltares (300 m length; 9.5 m depth; 5 m width, irregular waves up to Hs = 2 m)
- Asphalt plates, from Lauwersmeer dike, age 50 years, (8 x 0.5 m²) thickness 15 - 25 cm.
- On sand bed, with variable phreatic line.
- Wave loading in steps of 2 hours; two test series



Asphalt in series 1 had better quality and was less damaged than in series 2.

Density of sand bed in series 2 was typical for dike (proctor 90 -100); sand series 1 was less dense: proctor 85-90;

D50 sand = 240 µm.

8 asphalt plates cut from dike: 15 - 25 cm thick; and area 8 x 0.5 m²









Test series 1 and 2



Low phreatic line (both test series):

- 3 short duration tests (H_{m0} = 1 m)
- 3 tests: H_{m0} = 1.6 m; 1.8 m and 2.0 m (2 hours each)
- A few large single waves

High phreatic line (h_f = level):

- First series (better than average asphalt quality)
 - h_f = SWL, H_{m0} = 1.6 m (large damage after 1 hour)
- Second series (less than average asphalt quality)
 - $h_f = SWL 0.6 \cdot H_{m0}$, $H_{m0} = 2.0 \text{ m}$
 - $h_f = SWL 0.2 \cdot H_{m0}$, $H_{m0} = 2.0 \text{ m}$
 - h_f = SWL , H_{m0} = 2.0 m (large damage after 16 min.)

Failure at high phreatic line





Enabling Delta Life

Deltares

Low phreatic line; laser images



- Small deformation after 6 hours of wave action; no major damage.
- 6 hours is the typical duration of wave attack on the Lauwersmeer dike.

Modeling (phreatic line is low):

80 70

60

50 Druk [kPa]

40

30

20 10

0

-10 13

Single wave impact:

1. Abagus

2. Analytical formula's

Fatigue under storm conditions:

3. Model Wave impact (de Looff, A.K., et al., 2006. Proceedings ICCE 2006. San Diego, CA.)



Asphalt: thickness, E modulus, Poisson's

ratio, fatigue line; subsoil: modulus of subgrade reaction

(de Looff, A. K., et al., 2011. Proceedings of the Coastal Structures

2011 conference. Yokohama.)

Wave action: slope angle, triangular load, statistical distributions of factor of impact, width and impact position Main features input 1: pressure distribution as measured; linear elastic sand bed



Input modelling





Instrumentation





Typical wave attack with phreatic line low

afstand vanaf teenwaartse rand van asfaltplaat [m]





Pressure distribution on

Total stresses in

druk TSM's t.o.v. $t_0 \; [kN/m^2]$ druk DRO's t.o.v. talud $[kN/m^2]$ overzicht van golf 80 60 Pressure on slope 40 20 ſ -20 1917.5 1918 1918.5 1919 1919.5 1920 1920.5 1921 1921.5 1917 1922 tijd [s] 30 TSM41 (hooa) 20 TSM44 (**Total stresses** TSM45 (10 TSM46 (..... TSM42 (laag) 0 TSM43 (laag) 1917 1917.5 1918 1918.5 1919 1919.5 1920 1920.5 1921 1921.5 1922 tijd [s] druk WSM's [kN/m²] Ω ъĘ īЛ WSM26 WSM27 W -0.5 Pore water pressure -1 1917 1917.5 1918 1918.5 1919 1919.5 1920 1920.5 1921 1921.5 1922 tijd [s] rek t.o.v. t₀ [microrek] Rek05 20 Rek06 Rek07 10 Asphalt strains 0 -10 1918 1917.5 1918.5 1919 1919.5 1920 1920.5 1921 1921.5 1922 1917 tijd [s]

Time period = 6 seconds

Serie 2, golfklap 2, T15b (t_0 = 1916.687 s, t_1 = 1919.336 s, t_2 = t_{max} = 197

Results







• Factor of impact mostly lower than in standard model **High phreatic line:**

Failure within 1 hour of wave attack, mechanism uplift, no liquefaction

Low Phreatic line:

- Asphalt strains are up to factor 1 to 5 smaller than expected from Abaqus modeling
- Dynamic effects play a role: a shorter impact duration has less effect.
- In total: gain of an order of magnitude in time till failure (Miner's sum) might be possible.
- Further modelling is foreseen:
 - dynamics
 - visco-elastic asphalt

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