

Modeling Tide's Influence on Seawall's Surface Temperature in Tropical Regions

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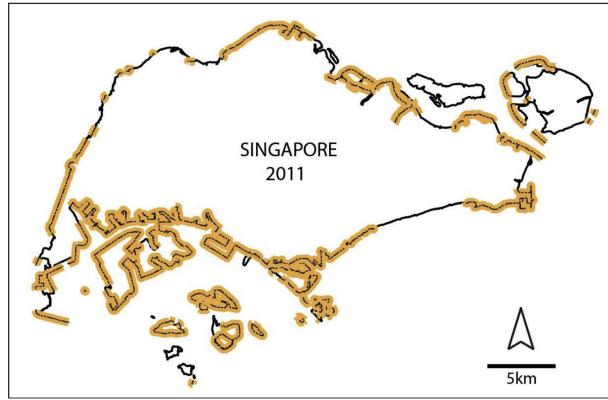




Introduction

Singapore's coastline and seawall

- Coastline 505 km
- Seawall 319 km
 - Granite
 - grouted
 - un-grouted
 - Vertical concrete



Data and Image from Lai et. al. (2015). The effects of urbanisation on coastal habitats and the potential for ecological engineering: A Singapore case study



Introduction

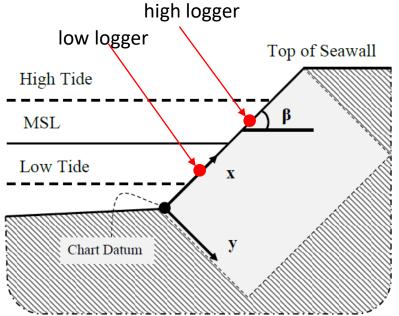
- Loss of natural habitat
- Redesign of seawalls
 - mitigating some negative impacts
 - improve their potential as a habitat
 - enhance biodiversity



- Why temperature (T)?
 - "Organisms living in the intertidal zone are faced with strong thermal stress given their cyclic exposure to air and immersion in water by tides." (Helmuth et al., 2002).
 - survival rate \searrow to zero, if T > 50 °C. (Somero, 2002).
 - seawall surface T can reach very high in tropical region, e.g., Singapore

Model extent

- Consider a seawall with 30° slope
 - a simple slope
 - x: parallel with seawall surface
 - y: perpendicular to seawall
 - chart datum: reference elevation
 - model extent: 8m x 5m
 - tidal range: 0.2m 3.2 m
 - \rightarrow range of x: 0.4m 6.4m
 - Element size: 0.05m x 0.05m
- Timestep, dt: 5 min
- Duration of calculation: 1 day





A suite of parameters



Weather				
Solar Radiation, Air Temperature, Wind Speed, Seawater Temperature	MPA Tide Record, Tide Table	Granite Seawall	Model	Т
		Thermal Properties, k, c, γ_{abs} , ϵ Density, ρ Geometry, ϕ , β , ω , γ , δ , θ	Boundary Condition, Initial Condition, Element size, Model Size,	

Theoretical Background

Image from Yang D. Solar Irradiance Modeling and Forecasting Using Novel Statistical Techniques

Heat equation

 $\rho c \frac{\partial T}{\partial t} = \frac{\partial}{\partial x} \left(k \frac{\partial T}{\partial x} \right) + \frac{\partial}{\partial y} \left(k \frac{\partial T}{\partial y} \right)$

- Deep boundary condition
 - no heat flow from deep ground
- Heat flux on surface
 - Solar radiation absorption
 - Long wave emission
 - Heat convection by air
 - Convection by seawater
- Initial temperature
 - 27°C at 0:00 am for Singapore.

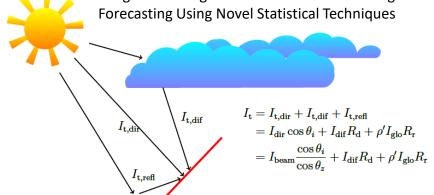


Fig. 1.3 Schematic diagram of various irradiance components received on a collector plane.

$$F_{y=0} = \begin{cases} q_{abs} + q_L + q_{conv,air}, \text{ above water} \\ q_L + q_{conv,sea}, \text{ under water} \\ q_{abs}(t) = \gamma_{abs} \cdot [q_{Ray} \cdot I_f + q_{DR} \cdot (\frac{1 + \cos \beta}{2})] \end{cases}$$

$$q_L = \sigma \times \epsilon \times (T_{sky}^4 - T_{sw}^4)$$

$$q_{conv,air} = h_{conv,air}(T_a - T_{sw})$$

$$q_{conv,sea} = h_{conv,sea}(T_{sea} - T)$$



Modelling method

- Finite Difference Method
 - central differencing

$$\rho c \frac{\partial T}{\partial t} = \frac{\partial}{\partial x} \left(k \frac{\partial T}{\partial x} \right) + \frac{\partial}{\partial y} \left(k \frac{\partial T}{\partial y} \right)$$

$$\downarrow$$

$$\rho c \left(\frac{T_{i,j} - T_{i,j}^{0}}{\Delta t} \right) = \theta \left[k \frac{T_{i+1,j} - 2T_{i,j} + T_{i-1,j}}{dx^2} + k \frac{T_{i,j+1} - 2T_{i,j} + T_{i,j-1}}{dy^2} \right]$$

$$+(1-\theta)\left[k\frac{T_{i+1,j}^{0}-2T_{i,j}^{0}+T_{i-1,j}^{0}}{dx^{2}}+k\frac{T_{i,j+1}^{0}-2T_{i,j}^{0}+T_{i,j-1}^{0}}{dy^{2}}\right]$$

- Crank-Nicolson scheme ($\theta = 0.5$)
- Treatment of boundary nodes
 - Ghost point technique (see next slide)

Modelling method

 T_N and T_{N-1} are used to find the flux equation on surface and then T_{N+1} . then T_{N+1} is put in the matrix to find T for all nodes. Iteration is required.

N-1

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y=0

dx

$$\rho c(\frac{T_{i,N} - T_{i,N}^{0}}{\Delta t}) = \theta [k \frac{T_{i+1,N} - 2T_{i,N} + T_{i-1,N}}{dx^{2}} + k \frac{T_{i,N+1} - 2T_{i,N} + T_{i,N-1}}{dy^{2}}]$$
Hux
$$+k \frac{T_{i,N+1} - 2T_{i,N}^{0} + T_{i-1,N}^{0}}{dx^{2}} + (1 - \theta) [k \frac{T_{i+1,N}^{0} - 2T_{i,N}^{0} + T_{i-1,N}^{0}}{dx^{2}} + k \frac{T_{i,N+1}^{0} - 2T_{i,N}^{0} + T_{i,N-1}^{0}}{dy^{2}}]$$
Ghost cell with $T_{i,N+1}$

$$F_{sw}|_{y=0} = k \frac{T_{i,N+1} - T_{i,N-1}}{2dy}$$
1. Initial guess of $T_{i,N}$
and $T_{i,N-1}$
2a. Find Fsw and $T_{i,N+1}$

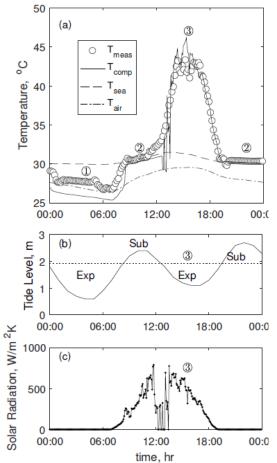
$$T_{i,N+1} = \frac{2dy}{k} \cdot F_{sw}|_{y=0} + T_{i,N-1}$$

$$F_{sw}|_{y=0} = \sigma \varepsilon (T_{sky}^4 - T_N^4) + \gamma_{abs} q_{SR} + h_{air} (T_{air} - T_N) + h_{sea} (T_{sea} - T_N)$$



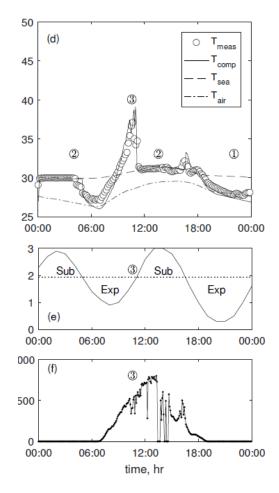
Results: seawall surface temperature

(a) low tide in the afternoon



- Three types of T
 - 1) exposed night
 - 2) submerged
 - 3) exposed daytime

(b) high tide in the afternoon



Model data comparison

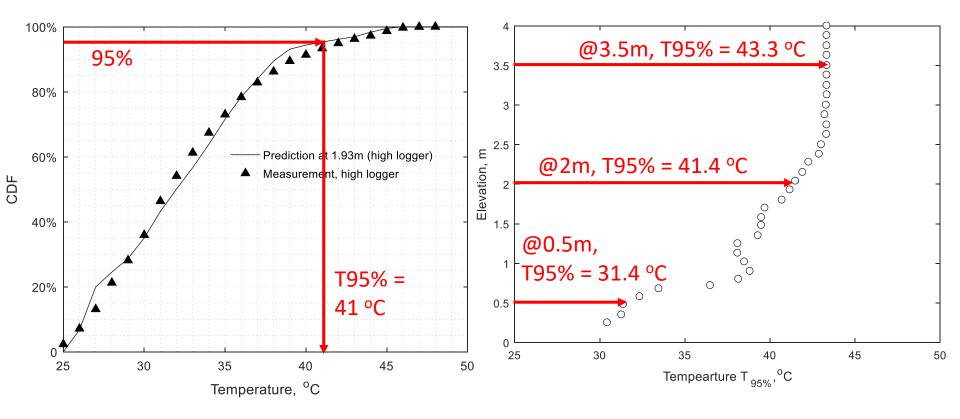


- Overall performance of model
 - 62% of data are within dashed lines: +- 2°C from perfect
- From the results of each elevation (e.g., at logger level in the figure), plot a cumulative distribution of T

Definition of local high temperature - T95%



- A term: T95% from numerical prediction
 - local high temperature, 95% of temperature do not exceed this threshold during exposed day time.



Model application – seawall slope



- Slope range in figure: 30 90 deg
- T95%, local high T
 - 90 deg slope is ~ 9 °C lower that of 30 deg slope
- Max solar radiation energy
 - Max SR for 90 deg slope is about half that of 30 deg slope seawall

Model application – seasonal effect



- Northeast monsoon
 - Dec, Jan, Feb
- Southwest monsoon
 - Jun, July, Aug, Sep
- Max Temperature difference: 5°C

Conclusion



- A finite difference model for seawall surface temperature
 - Absorption of solar radiation
 - Long wave emission
 - Convection by air and seawater
- Good agreement between prediction and field test
- Tide's cooling effects on the high temperature
- T95% local high temperature
- Effect of seawall slopes and seasons on T95%

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Q&A

Thank you!